City Care Milton Street Depot – Tradesmens Workshop Detailed Engineering Evaluation BU 1141-001 EQ2 Quantitative Report

Prepared for Christchurch City Council (Client)

By Beca Carter Hollings & Ferner Ltd (Beca)

4 October 2013

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Revision History

Revision Nº	Prepared By	Description	Date
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Document Acceptance

Action	Name	Signed	Date			
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City Care Milton Street Depot –Tradesmens Workshop BU 1141-001 EQ2

Detailed Engineering Evaluation Quantitative Report – SUMMARYVersion 1

Address 245 Milton Street Sydenham Christchurch



Background

This is a summary of the Quantitative Assessment report for the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) Revision 7 issued by the Engineering Advisory Group (EAG) in 2012.

A Qualitative Assessment report for the Tradesmens Workshop was issued to CCC on 7 June 2012

The Tradesmens Workshop is located at the City Care Milton St Depot at 245 Milton Street, Sydenham, Christchurch. It is a steel portal frame building with precast concrete shear walls. The structural drawings available indicate the Tradesmens Workshop was designed in 1974. Calculations have been undertaken as part of the Quantitative Assessment.

The format and content of this report follows a template provided by CCC, which is based on the EAG document.

Key Damage Observed

Visual inspections on 8 February 2012 and 9 October 2012 indicate the building has suffered moderate damage. Key damage observed include:

- Vertical cracking and spalling to the western and southern concrete walls adjacent to joints.
- Significant spalling to one columns' concrete encasement adjacent to the weld plate joints in the Sign Shop area. It was noted that this panel has been secured with steel brackets prior to our inspection.
- Diagonal cracking at the base of the concrete wall in the stairwell to the second storey office.
- Cracking and spalling to the column concrete encasement at various portal frame knee joints.
- Cracking to precast concrete wall panels at the portal frame knee cast in connections.

Critical Structural Weaknesses (CSW)

The following Critical Structural Weaknesses have been identified:

Site characteristics due to liquefaction occurring on the Milton St site.



 Difference in stiffness between the western Sign Shop area and the rest of the building due to the portal frame orientation.

Indicative Building Strength (from Detailed Assessment)

The building has been assessed to have a seismic capacity of 10%NBS in one localised area, using the New Zealand Society for Earthquake Engineering (NZSEE) Detailed Assessment guideline 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006, and is therefore Earthquake Prone and classified as Seismic Grade E.

Our assessment has identified the structural components that have governed/limited the building's seismic performance, and their potential failure mechanisms, are as follows:

- The beam supporting the southern Sign Shop portal frames achieve 10%NBS under longitudinal (out-of-plane) loading.
- The knee connection of the steel portal frames at the eastern end of the building achieve 35%NBS under transverse (in-plane) loading.
- The steel portal frame rafters at the eastern end of the building achieve 39%NBS under transverse (in-plane) loading.

There are a number of other elements in the building which have assessed seismic capacities greater than 33%NBS and less than 67%NBS.

The structural damage observed to the precast concrete panels is moderate and the seismic capacity of the precast concrete panels is considered to have reduced due to the damage from 100%NBS to 67%NBS. This reduction does not affect the overall seismic capacity of the building however, since this is limited by the Sign Shop portal frame support beam. No significant damage was noted to this element.

Recommendations

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be earthquake prone, having an assessed capacity less than 33%NBS, and is classified as Seismic Grade E. The risk of collapse of an earthquake prone building of this grade is considered to be more than 25 times greater than that of an equivalent new building.

For greater Christchurch the definition of a "dangerous" building in the Building Act has been extended (by the Canterbury Earthquake (Building Act) Order 2011) to include buildings at risk of collapsing in a moderate earthquake, that is earthquake prone buildings with a capacity at or below 33%NBS. Where council requires a dangerous building or an earthquake prone building to be upgraded, it may prohibit the use of the building until the works are carried out.

The structural damage observed to the precast concrete panels is moderate and the seismic capacity of the precast concrete panels is considered to have reduced due to the damage. This reduction does not affect the overall seismic capacity of the building. No significant damage was noted to the structural element that is the limiting capacity of the building.



It is recommended that:

- The immediate area under the southern Sign Shop portals is vacated or restricted use until local strengthening of the support beam is completed.
- The roof bracing in the trussed roof area should be installed as shown on the drawings.
- A full damage assessment is carried out for insurance purposes.
- A settlement survey could be carried out to determine the extent of settlement of the building for insurance purposes.
- According to the recent CCC Instructions to Engineers document (16 October 2012), Council's insurance provides for repairing damaged elements to a condition substantially as new. We suggest you consult further with your insurance advisor.



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1 Background

Beca Carter Hollings & Ferner Ltd (Beca) has been engaged by Christchurch City Council (CCC) to undertake a Quantitative Detailed Engineering Evaluation (DEE) of the Tradesmens Workshop building located at 245 Milton Street, Sydenham, Christchurch.

This report is a Quantitative Assessment of the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) Revision 7 issued by the Engineering Advisory Group in 2012.

A quantitative assessment involves analytical calculations of the building's strength and may involve material testing, geotechnical testing and intrusive investigation. The qualitative assessment previously carried out involved inspections of the building, a desktop review of existing structural and geotechnical information, including existing drawings and calculations, if available and an assessment of the level of seismic capacity against current code using the Initial Evaluation Procedure (IEP).

The purpose of these assessments is to determine the likely building performance and damage patterns, to identify any potential Critical Structural Weaknesses (CSW) or collapse hazards, and to make an assessment of the likely building strength in terms of percentage of New Building Standard (%NBS).

A full set of structural drawings (consent issue) was made available and has been used in our assessment of the building. The building description below is based on a review of the drawings and our visual inspections.

The format and content of this report follows a template provided by CCC, which is based on the EAG document.

2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

2.1 Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 - Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 – Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee carry out a full structural survey before the building is re-occupied.



We understand that CERA will require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building Act). It is understood that CERA is adopting the Detailed Engineering Evaluation Procedure document (draft) Revision 7 issued by the Engineering Advisory Group in 2012, which sets out a methodology for both qualitative and quantitative assessments. We understand this report will be used in response to CERA Section 51.

The qualitative assessment includes a thorough visual inspection of the building coupled with a desktop review of available documentation such as drawings, specifications and IEP's. The quantitative assessment involves analytical calculation of the building's strength and may require non-destructive or destructive material testing, geotechnical testing and intrusive investigation.

It is anticipated that factors determining the extent of evaluation and strengthening level required will include:

- The importance level and occupancy of the building
- The placard status that was assigned during the state of emergency following the 22 February 2011 earthquake
- The age and structural type of the building
- Consideration of any Critical Structural Weaknesses
- The extent of any earthquake damage

2.2 Building Act

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 – Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to any alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

Section 115 – Change of Use

This section requires that the territorial authority (in this case Christchurch City Council (CCC)) be satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'. Regarding seismic capacity 'as near as reasonably practicable' has previously been interpreted by CCC as achieving a minimum of 67%NBS however where practical achieving 100%NBS is desirable. The New Zealand Society for Earthquake Engineering (NZSEE) recommend a minimum of 67%NBS.

Section 121 – Dangerous Buildings

The definition of dangerous building in the Act was extended by the Canterbury Earthquake (Building Act) Order 2010, and it now defines a building as dangerous if:

- In the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
- In the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
- There is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a 'moderate earthquake' (refer to Section 122 below); or
- There is a risk that that other property could collapse or otherwise cause injury or death; or



 A territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.

Section 122 – Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property. A moderate earthquake is defined by the building regulations as one that would generate ground shaking 33% of the shaking used to design an equivalent new building.

Section 124 - Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 - Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

2.3 Christchurch City Council Policy

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake of the 4th September 2010.

The 2010 amendment includes the following:

- A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
- A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
- A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
- Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

It is understood that any building with a capacity of less than 33%NBS (including consideration of Critical Structural Weaknesses) will need to be strengthened to a target of 67%NBS of new building standard as recommended by the Policy.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply 'as near as is reasonably practicable' with:

- The accessibility requirements of the Building Code.
- The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

2.4 Building Code

The building code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.



On 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

- a. Hazard Factor increased from 0.22 to 0.3 (36% increase in the basic seismic design load)
- b. Serviceability Return Period Factor increased from 0.25 to 0.33 (80% increase in the serviceability design loads when combined with the Hazard Factor increase)

The increase in the above factors has resulted in a reduction in the level of compliance of an existing building relative to a new building despite the capacity of the existing building not changing.

3 **Earthquake Resistance Standards**

For this assessment, the building's Ultimate Limit State earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The new building standard load requirements have been determined in accordance with the current earthquake loading standard (NZS 1170.5:2004 Structural design actions - Earthquake actions - New Zealand).

No consideration has been given at this stage to checking the level of compliance against the increased Serviceability Limit State requirements.

The likely ultimate capacity of this building has been derived in accordance with the New Zealand Society for Earthquake Engineering (NZSEE) guidelines 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. These guidelines provide an Initial Evaluation Procedure that assesses a building's capacity based on a comparison of loading codes from when the building was designed and currently. It is a quick high-level procedure that can be used when undertaking a Qualitative analysis of a building. The guidelines also provide guidance on calculating a modified Ultimate Limit State capacity of the building which is much more accurate and can be used when undertaking a Quantitative analysis.

The New Zealand Society for Earthquake Engineering has proposed a way for classifying earthquake risk for existing buildings in terms of %NBS and this is shown in Figure 3.1 below.

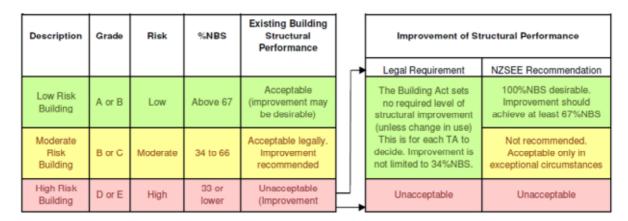


Figure 3.1: NZSEE Risk Classifications Extracted from Table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table 3.1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. on average 0.2% in any year). It is noted that the current seismic risk in Christchurch results in a 6% risk of exceedance in the next year.



Table 3.1: %NBS Compared to Relative Risk of Failure

Building Grade	Percentage of New Building Standard (%NBS)	Approx. Risk Relative to a New Building
A+	>100	<1
A	80-100	1-2 times
В	67-80	2-5 times
С	33-67	5-10 times
D	20-33	10-25 times
E	<20	>25 times

4 Building Description

4.1 General

Summary information about the building is given in the following table.

Table 4.1: Building Summary Information

Item	Details	Comment
Building name	City Care Milton Street Depot – Tradesmens Workshop	
Street Address	245 Milton Street Sydenham Christchurch	
Age	Designed in 1974, approved in 1977	From drawings available
Description	Series of workshops for the Sign Shop, Building Services and Plant Pool Hire, offices for City Care Facilities Management, and storage	
Building Footprint / Floor Area	Approx. 72.1m x 15.5m and 6.3m x 30.9m. 1310m ² internally	
No. of storeys / basements	Mostly 1 storey/no basement	Mezzanine storage floors in eastern workshop area. Second storey office above building services workshop
Occupancy / use	Workshops, offices and storage	Importance Level 2
Construction	Steel portal frames with glazed infill's and concrete walls	
Gravity load resisting system	Steel roof onto steel purlins, which are supported by steel portal frames	



Item	Details	Comment
Seismic load resisting system	Steel portal frames transversely with precast concrete shear walls longitudinally. Steel cross bracing in the roof. The direction of each system changes at the western end of the building.	The drawings indicate roof bracing in the trussed roof area of the building between gridlines 7 and 9. Site inspections revealed that only one of the bays of bracing was constructed in accordance with the drawings. Site inspections also revealed that the internal precast concrete wall along gridline 3 was also not constructed. These items have not been included in this assessment.
Foundation system	Reinforced concrete slab with concrete pads and tie beams.	Inferred from drawings.
Stair system	Timber stairs to upstairs office.	
Other notable features	Mezzanines at eastern end of building.	
External works		
Construction information	Structural drawings by City Engineer's Department dated 1974 and partial Architectural drawings by Lucking and Vial. Both consent copies dated 1977.	
Likely design standard	NZSS 1900, Chapter 8:1965	Inferred from age of building.
Heritage status	No known heritage status	
Other	Steel framed silo support adjacent to Building Services workshop.	Not attached and not considered part of the building.

4.2 Structural 'Hot-spots'

Areas in which damage may be expected to occur from earthquake shaking are outlined below;

- Precast concrete wall panels and column encasements due to out-of-plane movement.
- Cast-in wall connections to the portal frame column.
- Elements in the area where the Sign Shop and the main workshop area meet.
- Southern precast concrete wall panels orthogonal to the panels supporting the office mezzanine due to stiffness incompatibility between portal frames.
- Roof bracing connections.
- Connections between the Sign Shop portal frames and their support beam on gridline 2.



5 Site Investigations

5.1 Previous Assessments

It is understood that Opus International Consultants undertook rapid assessments of the buildings on the Milton St Depot site. These reports were not available for review. City Care carried out a damage assessment in April 2011 (refer Appendix D).

Visual inspections as part of the Level 4 assessment were undertaken on 8 February 2012. A Qualitative Report was issued to CCC on 7 June 2012.

5.2 Level 5 Intrusive Investigations

A further inspection was carried out on 9 October 2012 as part of the Level 5 Quantitative Assessment. This inspection revealed the missing bay of roof bracing in the trussed roof area.

6 Damage Assessment

6.1 Damage Summary

The table below provides a summary of damage that we observed on our inspection visit. Refer to Appendix A for photographs.

Table 6.1: Damage Summary

Damage type	Unknown	Minor	Moderate	Major	Comment
settlement of foundations	✓				None observed during visual inspection. Level survey may be required to confirm.
tilt of building	✓				No visual observation noted during visual inspection. Verticality survey may be required to confirm.
liquefaction		✓			None observed during visual inspection. Contacts on site stated it had occurred in areas throughout the site. The aerial reconnaissance on 24 Feb 2011 indicates the extent was minor.
settlement of external ground					None observed during visual inspection.
lateral spread / ground cracks					None observed during visual inspection.
frame			*		Damage to a columns concrete encasement in the Sign Shop, possibly indicating pull-out of the panel connection, was observed. This was temporarily repaired prior to our visual inspections. Various other column concrete encasements had minor cracking and some spalling at the
					top of the encasement at the portal knee was observed.



Damage type	Unknown	Minor	Moderate	Major	Comment
concrete walls			✓		Cracking and some spalling adjacent to the joints and connections of the precast concrete panels was observed. Minor diagonal cracking to the concrete walls of the second storey office and the Plant Hire area was observed.
cracking to concrete floors	1				None observed during inspection, however some areas could not be viewed due to carpet, heavy machinery and equipment etc.
bracing					No damage was observed during our visual inspection.
precast flooring seating					No damage was observed during our visual inspection.
stairs					No damage was observed during our visual inspection.
cladding /envelope		✓			Cracking to precast concrete wall panels observed as described above
internal fit out		✓			Minor plasterboard cracking observed.
building services	✓				No inspections of services were carried out.
adjacent building					No adjacent buildings are close enough to affect this building in an earthquake.
other					

6.2 Surrounding Buildings

There are no adjacent structures that are close enough that they may affect the Tradesmens Workshop during an earthquake.

The steel frame silo support adjacent to the Building Services Workshop has not been considered part of the building for the assessment. It is not attached to the Trademsens Workshop structure and a separate assessment may be required. No damage was observed to this during the visual inspection.

6.3 Residual Displacements and General Observations

No evidence of permanent settlement or displacements was observed during our visual inspection, however a global settlement survey may reveal movement that could be described as damage under insurance entitlement.

6.4 Implication of Damage

The structural damage observed to the precast concrete panels is moderate and the seismic capacity of the precast concrete panels is considered to have reduced due to the damage from 100%NBS to 67%NBS. This reduction does not affect the overall seismic capacity of the building



which is governed by the assessed capacity of the portal frame support beam, above the Sign Shop.

Where temporary works have been installed a full 'as new' repair, including strengthening as required, will need to be designed and constructed. A Building Consent will be required for any structural repair or strengthening. Fire and Access reports will also be required as part of the Building Consent process and a geotechnical report may also be required.

7 Generic Issues

The following generic issues referred to in Appendix A of the EAG guideline document have been identified as applicable to the Tradesmens Workshop building:

Single Level Tilt Panel

- Brittle panel connections and/or cracked panels at the connections.
- Panel span/thickness ratio too high, leading to panel buckling concerns.
- Steel bracing in adequate.

Welded and Bolted Steel Moment Frames

Inadequate stiffness as a whole meaning the building exceeds drift limits.

8 Geotechnical Consideration

No geotechnical information was available for this site. During the inspection, no damage to the surrounding pavement was noted and no effect to the structure was considered.

9 Survey

No level or verticality surveys were carried out as there was no visible evidence of settlement or displacement observed during the inspection. CCC may wish to undertake a level survey as part of insurance entitlement considerations.

A spirit level 'plumb' check should be done as a minimum as part of the full damage inspections.

10 Detailed Seismic Capacity Assessment

10.1 Assessment Methodology

The building has had its seismic capacity assessed using the Forced-based Detailed Assessment Procedures in the NZSEE 2006 AISPBE guidelines, based on the drawings and visual inspections.

The structure has suffered moderate damage to the precast concrete panels. The post-damage capacity of the panels is considered to be less than the original capacity, however this does not affect the overall seismic capacity of the building.

10.2 Assumptions

The following assumptions were used in our quantitative assessment:



- Reinforcing steel yield strength f_v = 275 MPa (as noted on the drawings)
- Concrete compressive strength f_c' = 25 MPa (as noted on the drawings)
- Structural steel yield strength f_v = 250 MPa
- Timber diaphragm strength of 5kN/m (as suggested in the NZSEE 2006 AISPBE guidelines)

10.3 Critical Structural Weaknesses

The following Critical Structural Weaknesses have been identified:

- Site characteristics due to liquefaction occurring on the Milton St site
- Difference in stiffness between the western Sign Shop area and the rest of the building.

The site characteristics have been identified as a potential CSW in our earlier Qualitative Report. We note that liquefaction is still considered a potential CSW however has not been considered in this quantitative assessment as we believe it will not have a direct impact on the structure's ability to resist further loads or cause global failure of the structure.

The two areas have similar lateral load resisting systems, orientated in orthogonal directions. This will result in the buildings responding differently in each load direction and may be the cause of the damage to column in the Sign Shop area.

10.4 Seismic Parameters

The seismic design parameters based on current design requirements from NZS 1170.5:2004 and the NZBC clause B1 for this building are:

- Site soil class: D NZS 1170.5:2004, Clause 3.1.3, Soft Soil
- Site hazard factor, Z = 0.3 NZBC, Clause B1 Structure, Amendment 11 effective from 19 May 2011
- Return period factor Ru = 1 NZS 1170.5:2004, Table 3.5, Importance Level 2 structure with a 50 year design life.
- Near fault factor N(T,D) = 1 NZS 1170.5:2004, Clause 3.1.6, Distance more than 20 km from fault line.

10.5 Results of Seismic Assessment

The results of our quantitative assessment indicate the building has a seismic capacity in the order of 10%NBS. This is lower than the IEP assessment of 36%NBS in the previous Qualitative Report. Table 10.1 presents the evaluated seismic capacity in terms of %NBS of the individual structural systems and components in each building direction.

Table 10.1: Summary of Seismic Assessment of Structural Systems

Item	Loading Direction	Ductility, μ	Seismic Performance	Notes
Overall %NBS adopted from DEE	Longitudinal	1.25	10%NBS	Governed by weak axis bending of the Sign Shop portal frame support beam
Portal frames – main area	Transverse	1.25	39%NBS	Eastern portal frame rafters in flexure
Portal frame connections – main area	Transverse	1.25	35%NBS	Knee connection stiffener yield capacity



Item	Loading Direction	Ductility, μ	Seismic Performance	Notes
Portal frames – Sign Shop area	Longitudinal	1.25	57%NBS	Excessive deflection of the northern frames
Portal frame connections – Sign Shop area	Longitudinal	1.25	67%NBS	Knee connection stiffener yield capacity
Frames connecting the Sign Shop and main areas	Longitudinal	1.25	10%NBS	Weak axis bending of beam supporting Sign Shop portal frames
Precast panel, in- plane capacity	Longitudinal	1.25	69%NBS	Uplift resistance of foundations
Precast panel connections (damaged)	Longitudinal	1.0	67%NBS	Shear capacity of damaged welded connections under inplane loading
Precast panel, out- of-plane capacity (damaged)	Both	1.25	100%NBS	Precast panels have been analysed as a part. Damaged connections have lost some resilience, however still achieve 100%NBS
Roof bracing and connections	Longitudinal	1.0	41%NBS	Tension capacity of flat bracing in main area
Two-storey office area walls	Longitudinal	1.25	96%NBS	Uplift resistance of foundations
Two-storey office area connections	Both	1.0	100%NBS	Between precast floor units and precast walls
Steel trussed roof area	Longitudinal	1.25	89%NBS	Minor axis bending of portal frame rafters supporting transverse PC panels
Southern mezzanine	Longitudinal	1.25	77%NBS	Flexural capacity of the columns
Main mezzanine	Longitudinal	1.25	100%NBS	Moment resisting steel frames
	Transverse	3.0	100%NBS	Timber floor diaphragm
Eaves beam	Longitudinal	1.25	66%NBS	Axial compression

Note: Ductility factors are in accordance with values recommended in the NZSEE 2006 AISPBE guidelines.

10.6 Discussion of results

The key findings of the assessment are as follows:

- The beam supporting the southern Sign Shop portal frames achieve 10%NBS under longitudinal (out-of-plane) loading.
- The knee connection of the steel portal frames at the eastern end of the building achieve 35%NBS under transverse (in-plane) loading.



The steel portal frame rafters at the eastern end of the building achieve 39%NBS under transverse (in-plane) loading.

There are a number of other elements in the building which have assessed seismic capacities greater than 33%NBS and less than 67%NBS.

Based on the results of our Quantitative Assessment, the Tradesmens Workshop is considered Earthquake Prone, as the seismic capacity was assessed to be less than 33%NBS, and is classified as Seismic Grade E.

11 **Recommendations**

11.1 Occupancy

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be earthquake prone, having an assessed capacity less than 33%NBS, and is classified as Seismic Grade E. The risk of collapse of an earthquake prone building of this grade is considered to be more than 25 times greater than that of an equivalent new building.

For greater Christchurch the definition of a "dangerous" building in the Building Act has been extended (by the Canterbury Earthquake (Building Act) Order 2011) to include buildings at risk of collapsing in a moderate earthquake, that is earthquake prone buildings with a capacity at or below 33%NBS. Where council requires a dangerous building or an earthquake prone building to be upgraded, it may prohibit the use of the building until the works are carried out.

The structural damage observed to the precast concrete panels is moderate and the seismic capacity of the precast concrete panels is considered to have reduced due to the damage. This reduction does not affect the overall seismic capacity of the building. No significant damage was noted to the structural element that is the limiting capacity of the building. Vacate the immediate area under the southern Sign Shop portals until the support beam is strengthened.

11.2 Further Investigations, Survey or Geotechnical Work

It is recommended that:

- The immediate area under the southern Sign Shop portals is vacated or restricted use until local strengthening of the support beam is completed.
- The roof bracing in the trussed roof area should be installed as shown on the drawings.
- A full damage assessment is carried out for insurance purposes.
- A verticality survey could be carried out to determine the extent of movement of the building for insurance purposes. A spirit level 'plumb' check should be done as a minimum as part of the full damage inspections.

11.3 **Damage Reinstatement**

According to the recent CCC Instructions to Engineers document (16 October 2012), Council's insurance provides for repairing damaged elements to a condition substantially as new. We suggest you consult further with your insurance advisor.



12 Design Features Report

Repairs will be required to reinstate the existing structural system. A repair methodology has not been prepared at this stage. No new load paths are expected as a result of the repairs required.

13 Limitations

The following limitations apply to this engagement:

- Beca and its employees and agents are not able to give any warranty or guarantee that all defects, damage, conditions or qualities have been identified.
- Inspections are primarily limited to visible structural components. Appropriate locations for invasive inspection, if required, will be based on damage patterns observed in visible elements, and review of the construction drawings and structural system. As such, there will be concealed structural elements that will not be directly inspected.
- The inspections are limited to building structural components only.
- Inspection of building services, pipework, pavement, and fire safety systems is excluded from the scope of this report.
- Inspection of the glazing system, linings, carpets, claddings, finishes, suspended ceilings, partitions, tenant fit-out, or the general water tightness envelope is excluded from the scope of this report.
- The assessment of the lateral load capacity of the building is limited by the completeness and accuracy of the drawings provided. Assumptions have been made in respect of the geotechnical conditions at the site and any aspects or material properties not clear on the drawings. Where these assumptions are considered material to the outcome further investigations may be recommended. It is noted the assessment has not been exhaustive, our analysis and calculations have focused on representative areas only to determine the level of provision made. At this stage we have not undertaken any checks of the gravity system, wind load capacity, or foundations.
- The information in this report provides a snapshot of building damage at the time the detailed inspection was carried out. Additional inspections required as a result of significant aftershocks are outside the scope of this work.

This report is of defined scope and is for reliance by CCC only, and only for this commission. Beca should be consulted where any question regarding the interpretation or completeness of our inspection or reporting arises.



Appendix A

Photographs

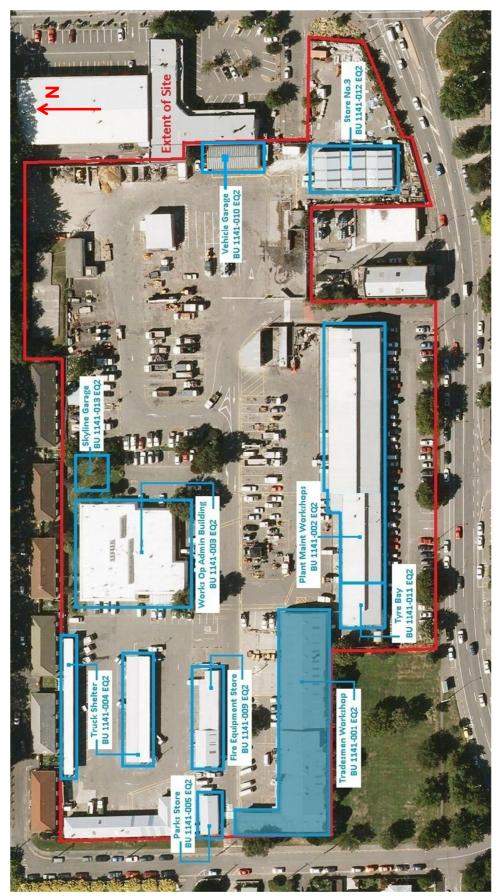


Figure 1A: Site Layout (North is to left of page)



Photo 1: Exterior view of Sign Shop and Building Services Workshop (North-west elevation)



Photo 2: Exterior view of Facilities Management (North elevation)



Photo 3: Exterior view of Hire Pool / Storage / Weed Spraying areas (North-east elevation)

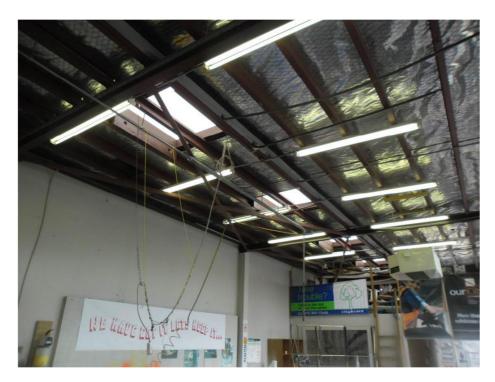


Photo 4: Interior view of Sign Shop



Photo 5: Interior view of Building Services Workshop



Photo 6: Interior view of Hire Pool / Storage / Weed Spraying areas

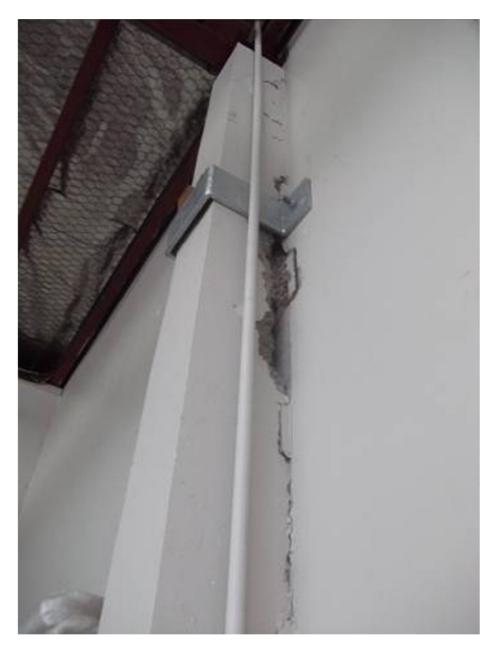


Photo 7: Damage to column encasement

Damage Description: Possible pull out of connection causing damage to column encasement, with temporary repair bracket



Photo 8: Damage to wall on other side of Photo 7.

Damage Description: Possible pull out of connection causing damage to column encasement, with temporary repair bracket



Photo 9: Cracking to concrete wall panel

Damage Description: Cracking to concrete wall panel adjacent to movement joint



Photo 10: Typical cracking to concrete wall panel

Damage Description: Cracking to concrete wall panel at bottom corner adjacent to movement joint



Photo 11: Typical cracking to concrete wall panel

Damage Description: Cracking to concrete wall panel protruding from weld plate at portal knee



Photo 12: Cracking to concrete wall

Damage Description: Diagonal crack to concrete wall in stairwell



Photo 13: Cracking to concrete wall

Damage Description: Cracking to concrete panels in Plant Hire area protruding from doorway



Photo 14: Cracking to concrete wall

Damage Description: Cracking to concrete panels in Plant Hire area by doorway

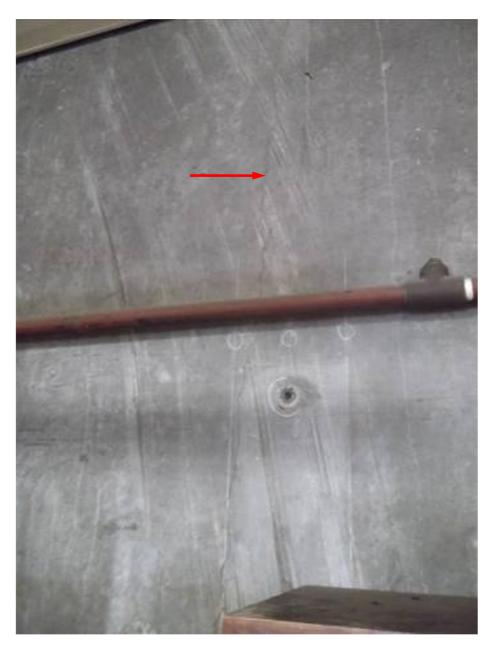


Photo 15: Cracking to concrete wall

Damage Description: Cracking to concrete panels in Plant Hire area

Appendix B

Existing Drawings

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CONTRAL DEPOT.

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with regulations of

CHRISTCHURCH

PLAN NO.

LETTER REF.

DRAINAGE BOARD

STAGE 1
NEW CENTRAL DEPOT JOHNSON ST. SYDENHAM
FOR THE CHRISTCHURCH CITY COUNCIL

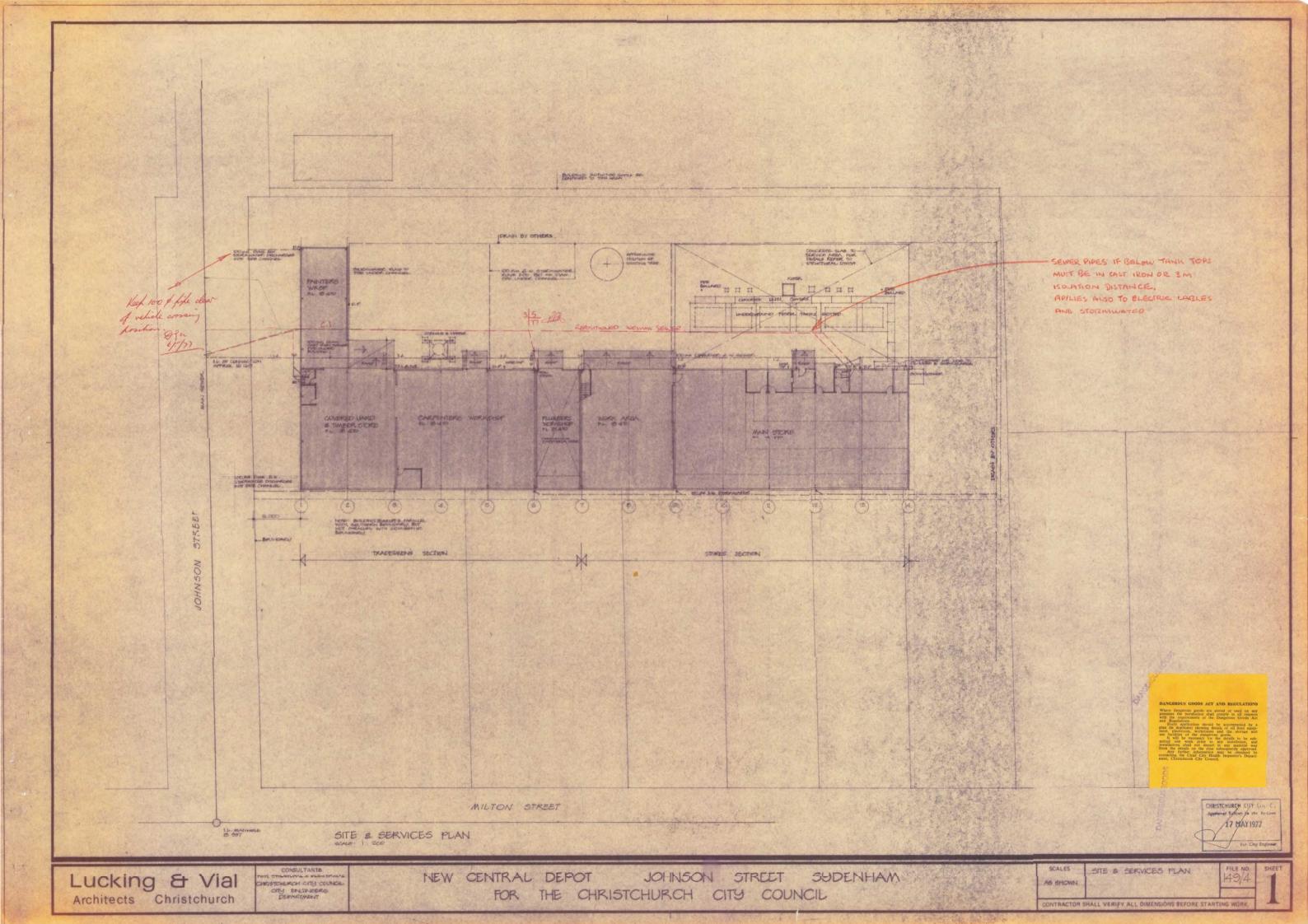
architects

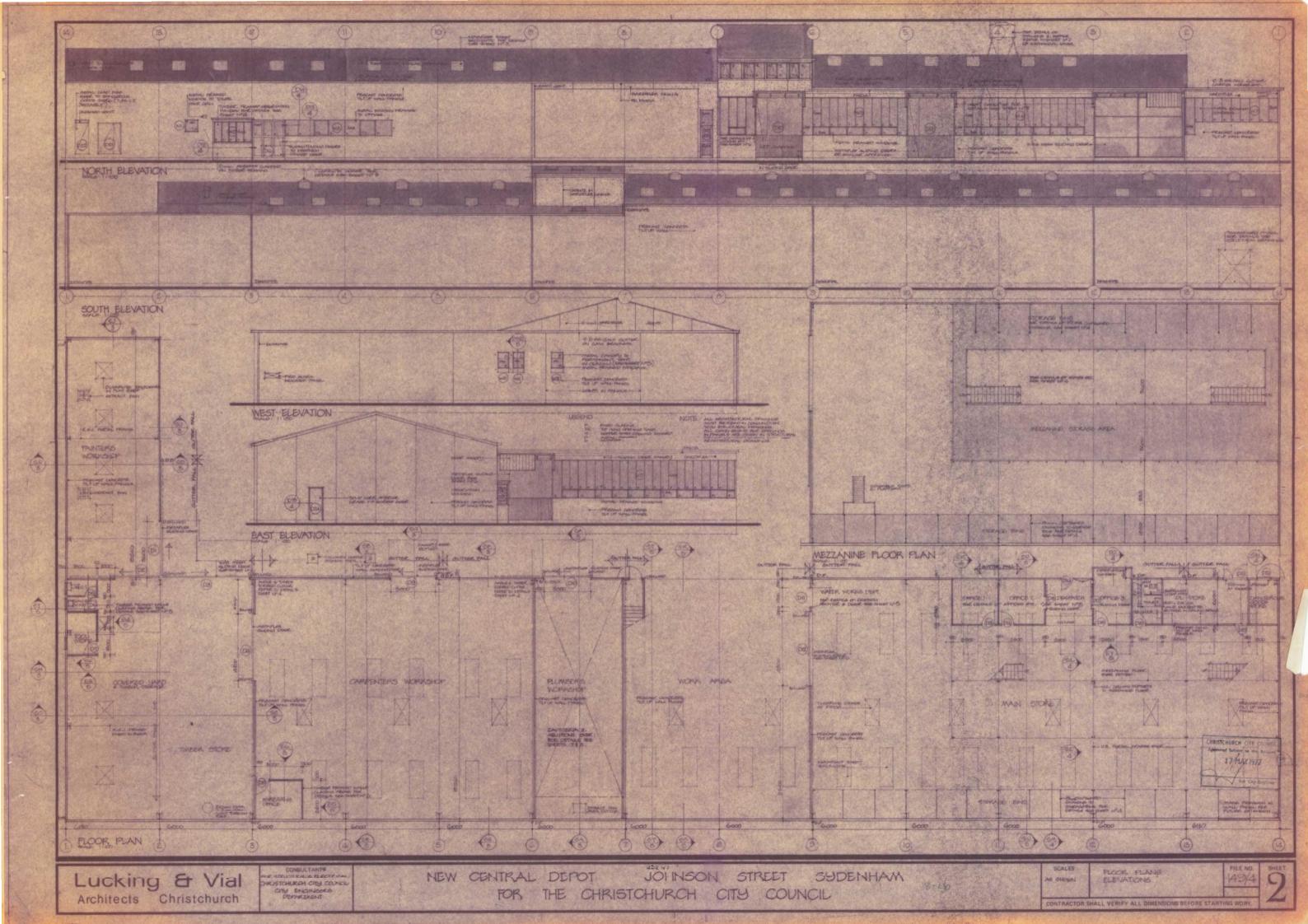
LUCKING & VIAL CHRISTCHURCH

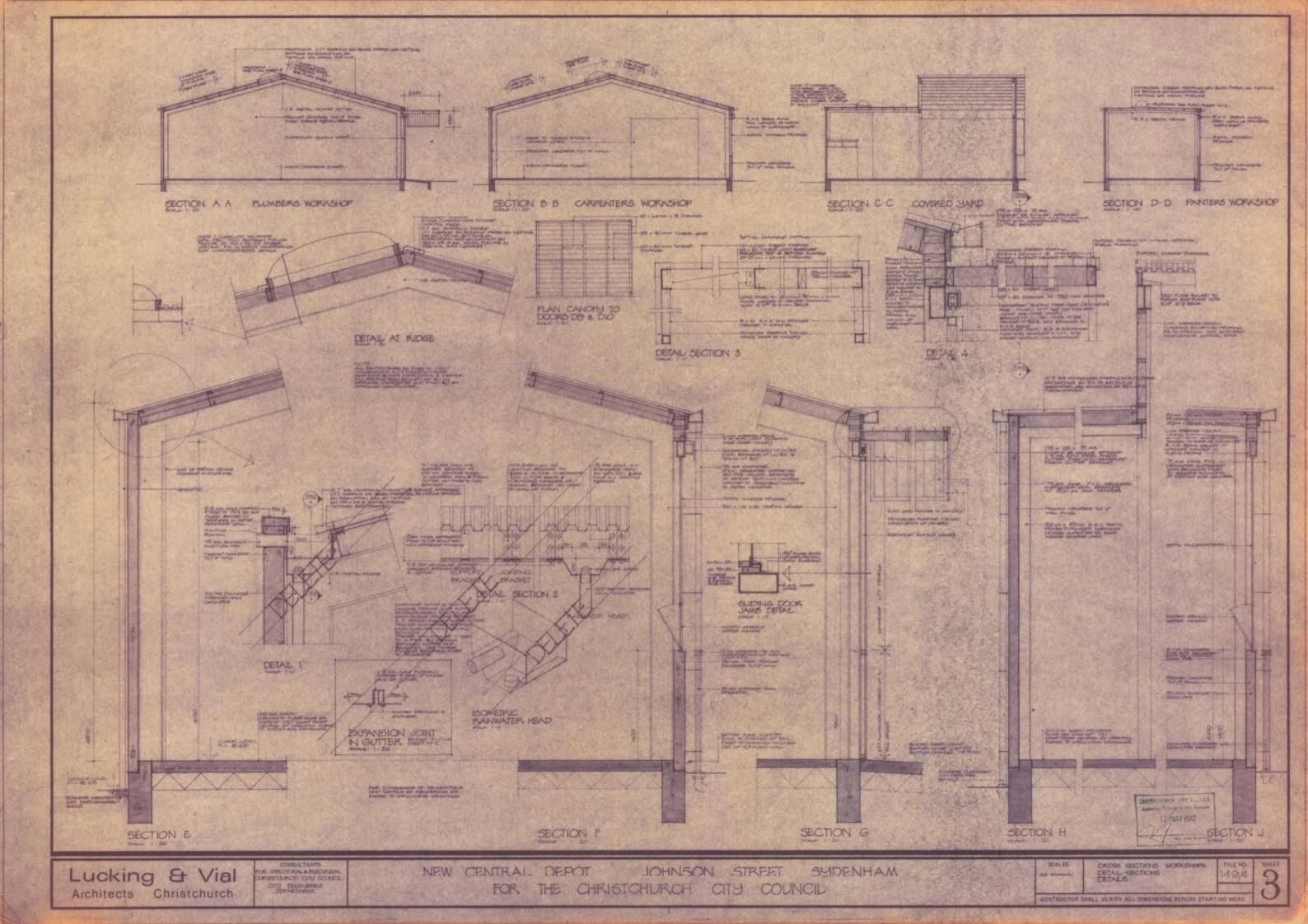
structural & electrical engineer CHRISTCHURCH CITY COUNCIL CITY ENGINEERS DEPARTMENT

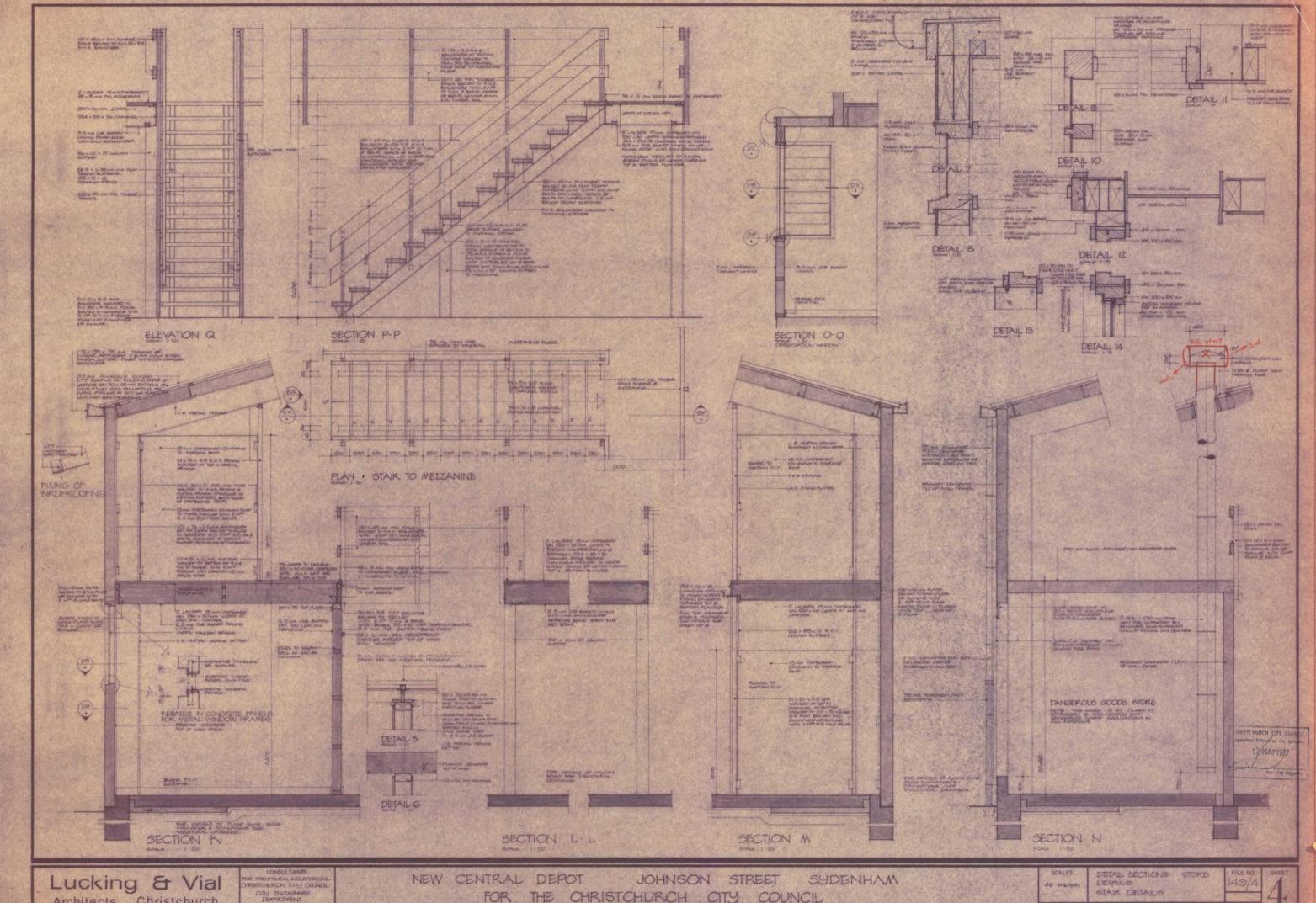
quantity surveyor

CHRISTCHURCH CITY COUNCIL CITY ENGINEERS DEPARTMENT



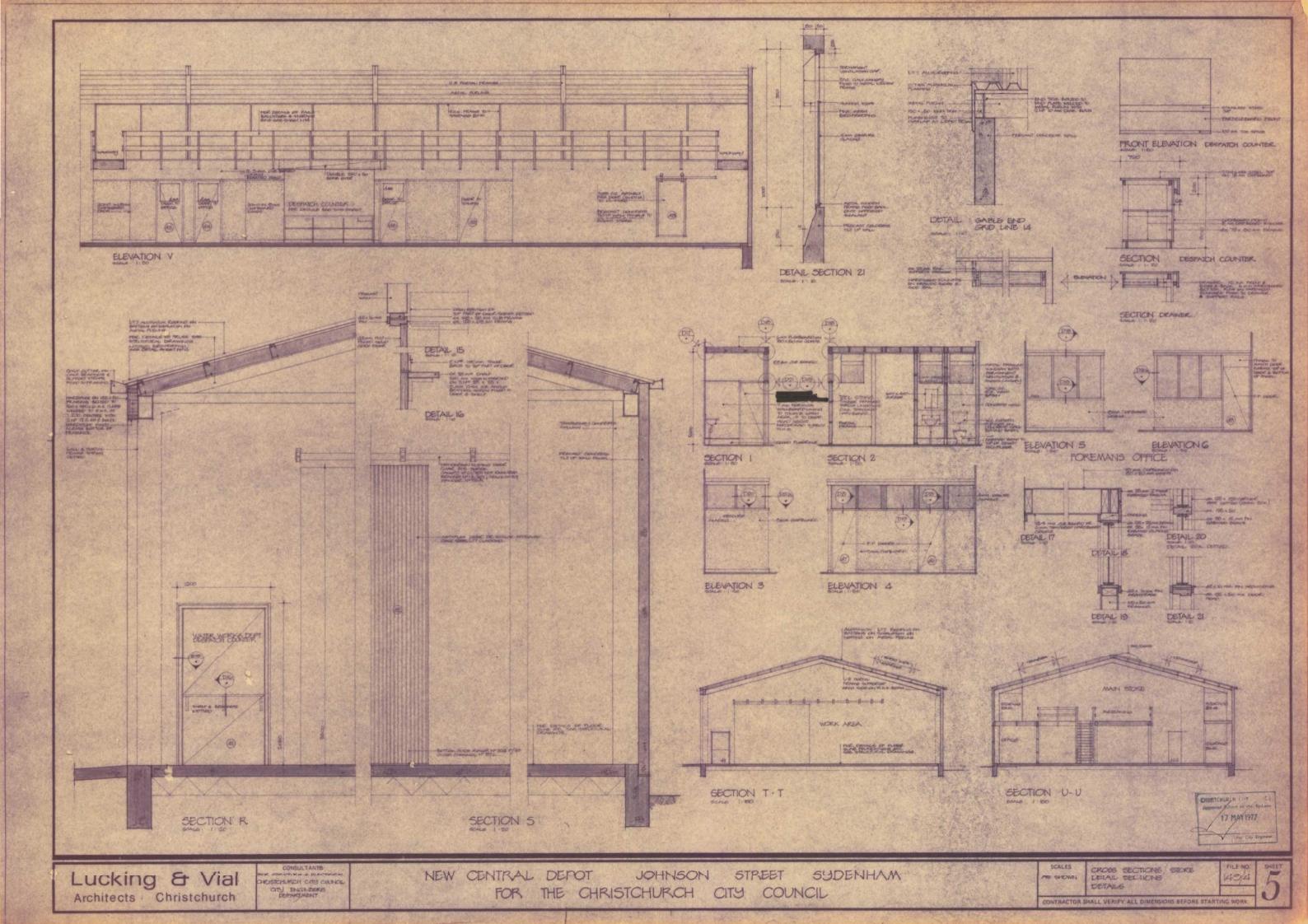


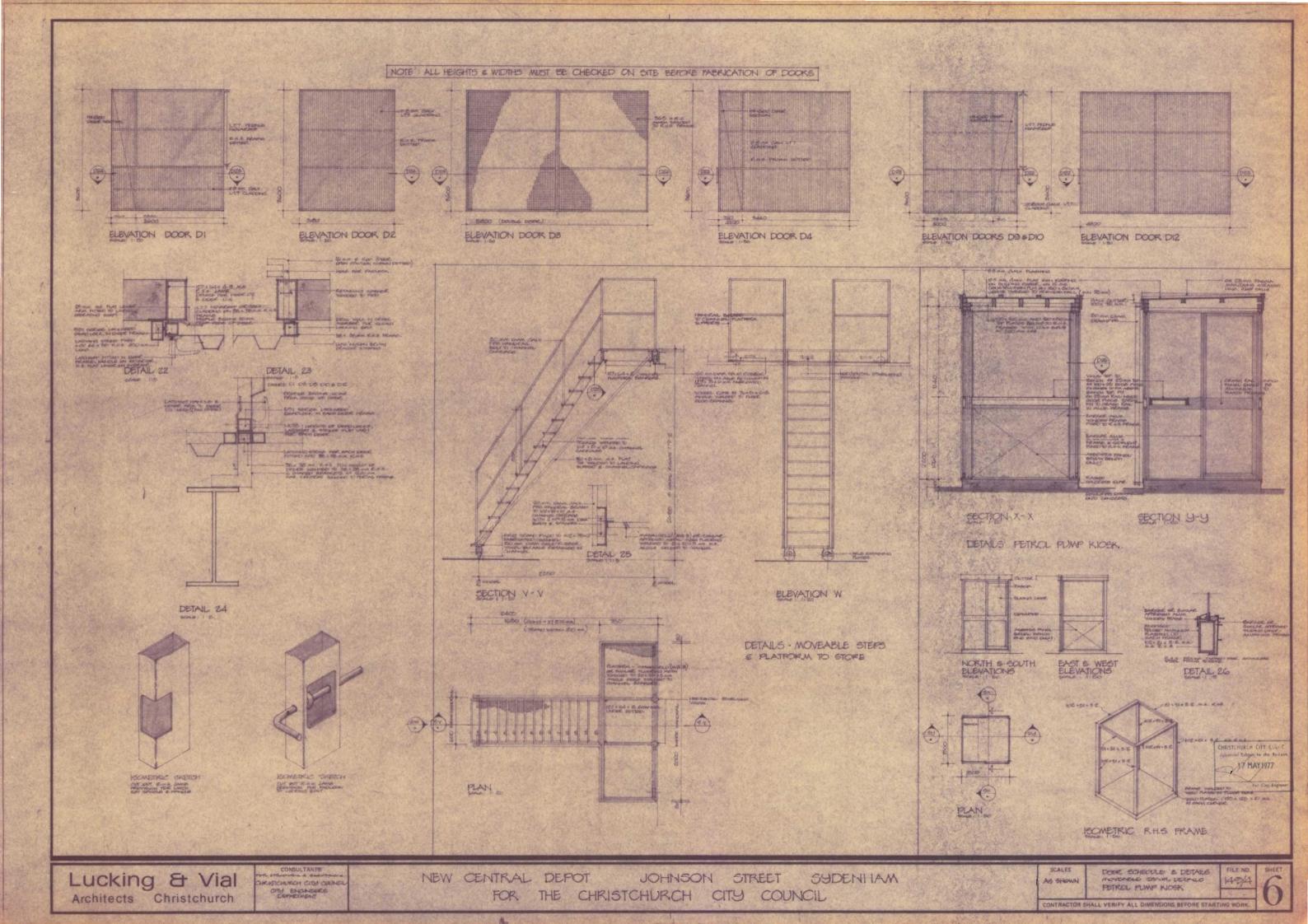


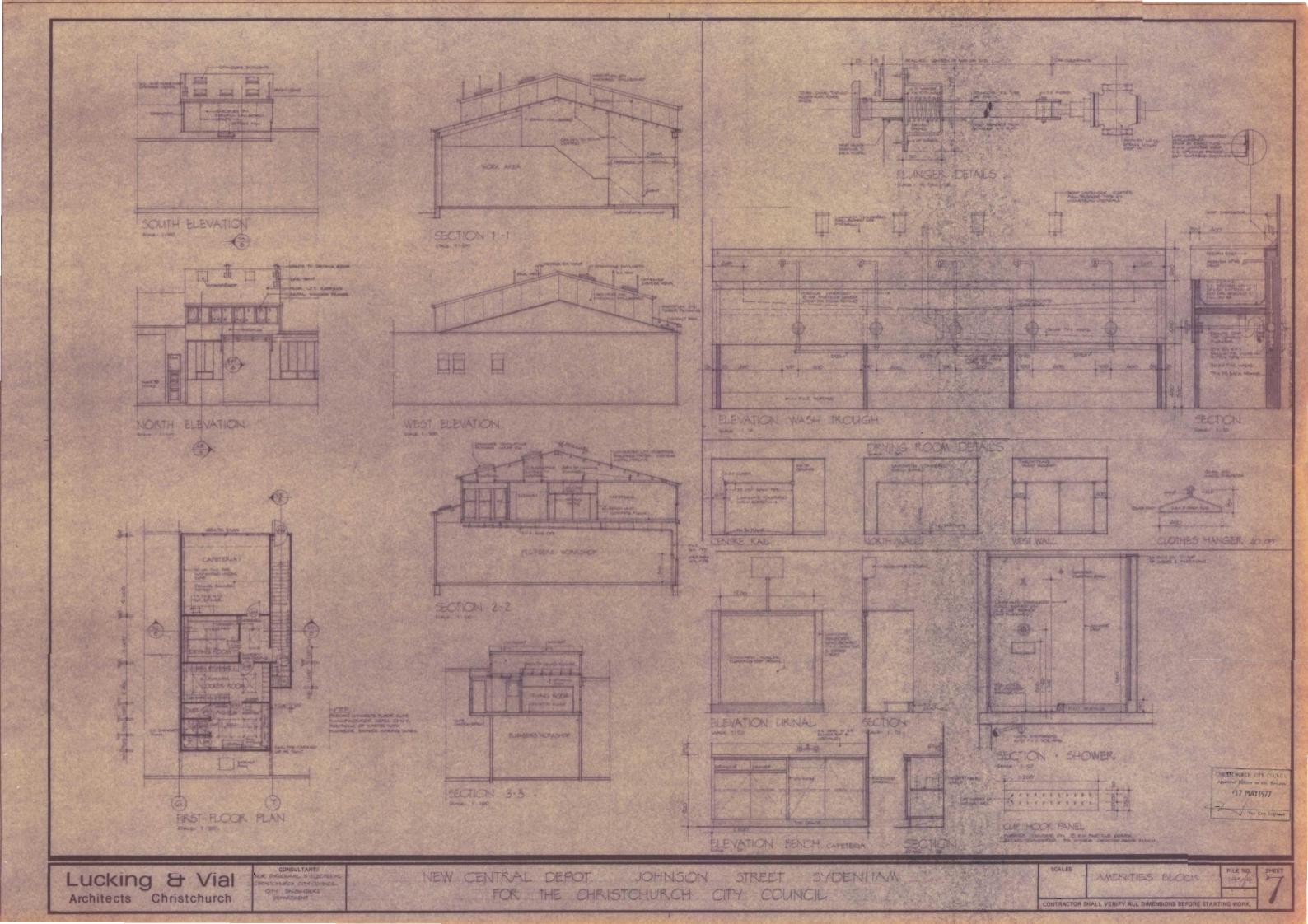


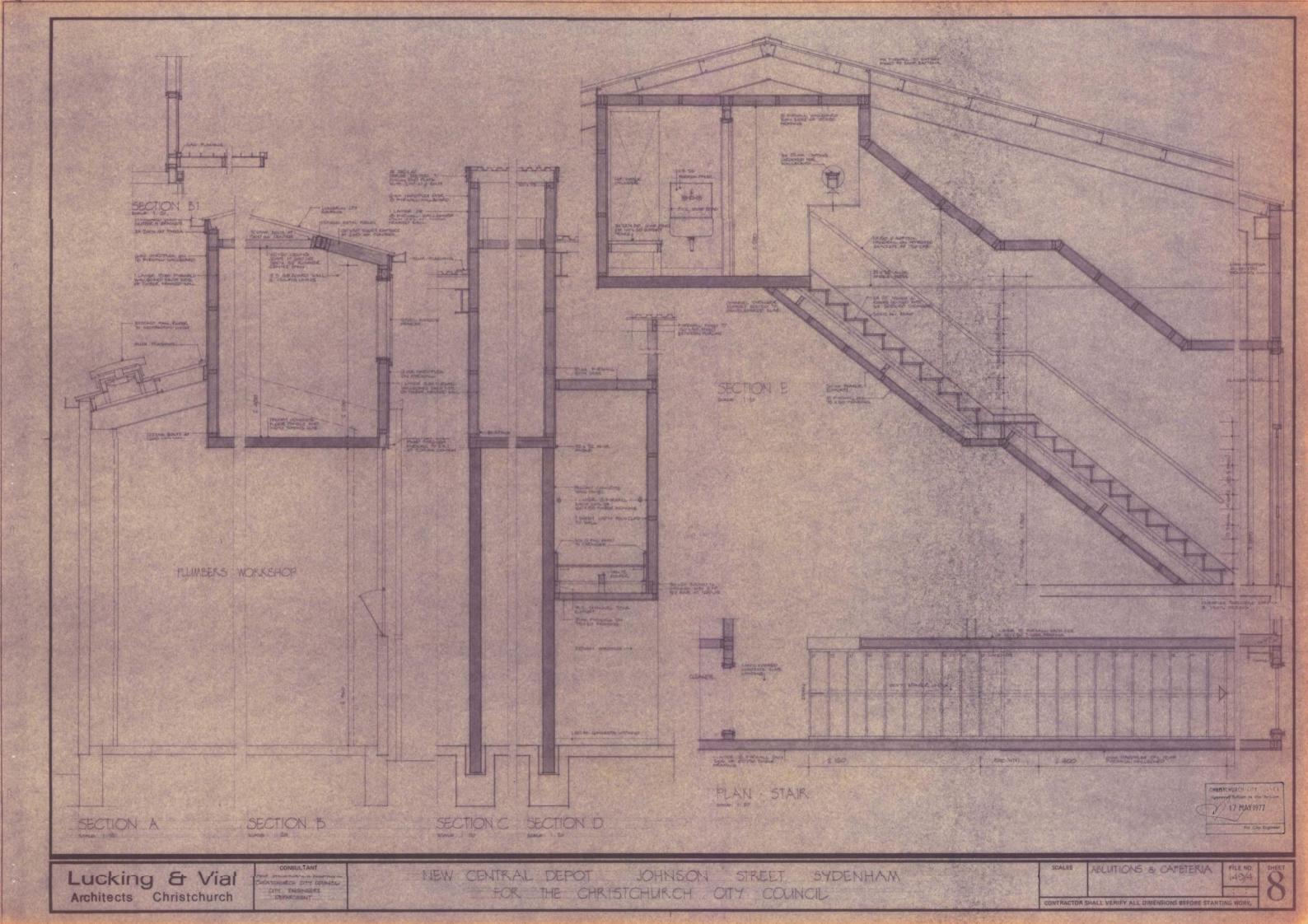
Architects Christchurch

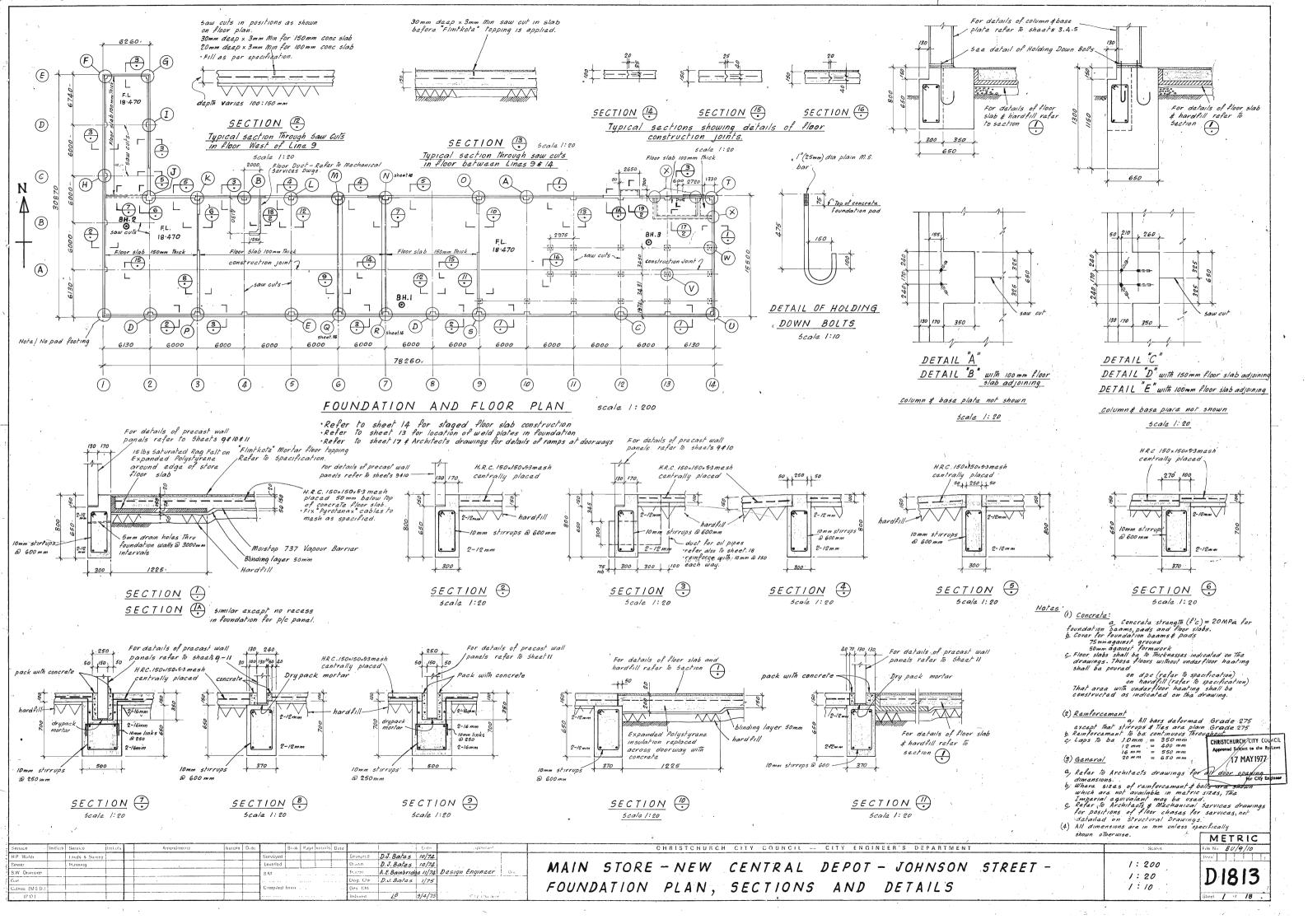
FOR THE CHRISTCHURCH CITY COUNCIL

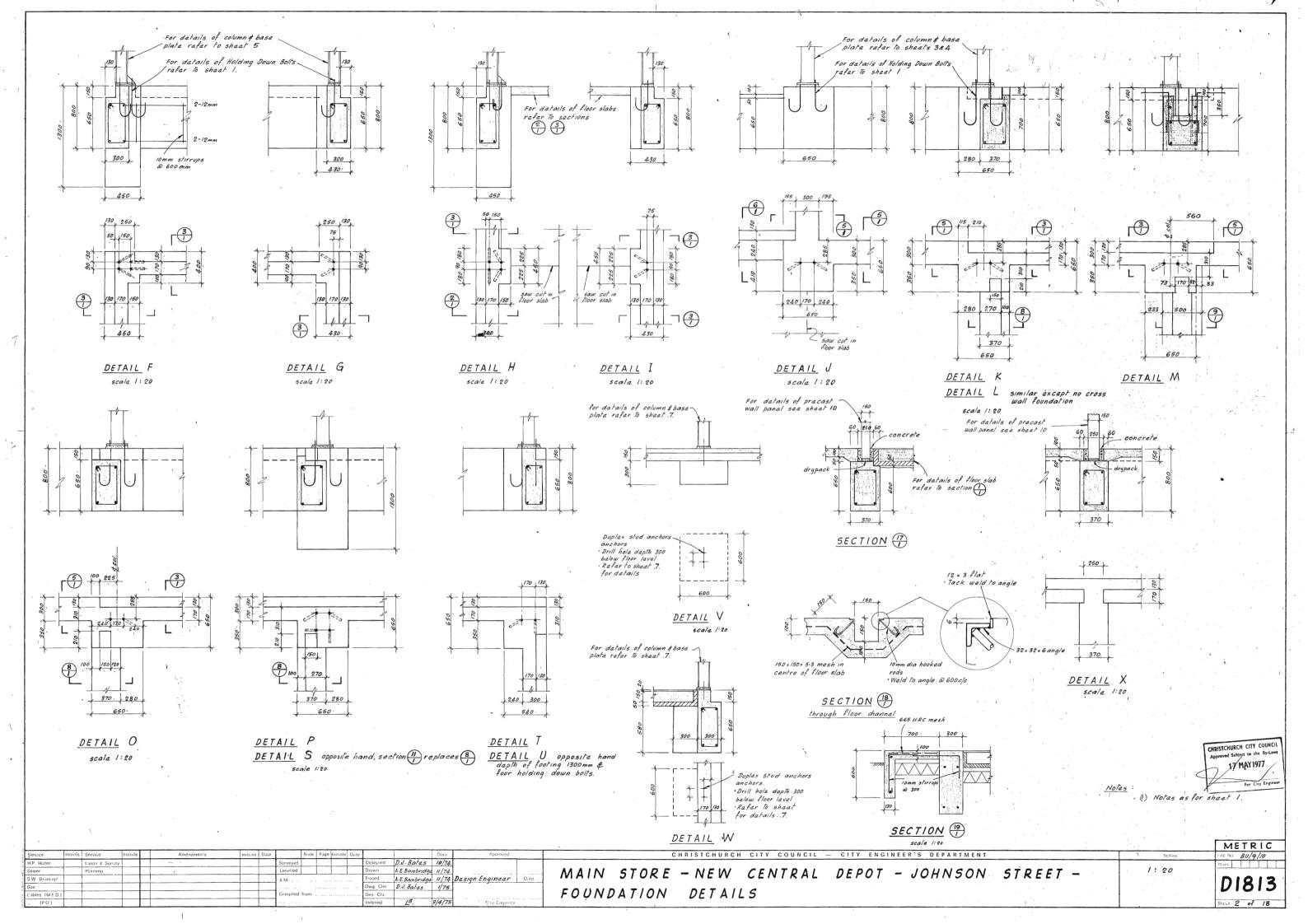


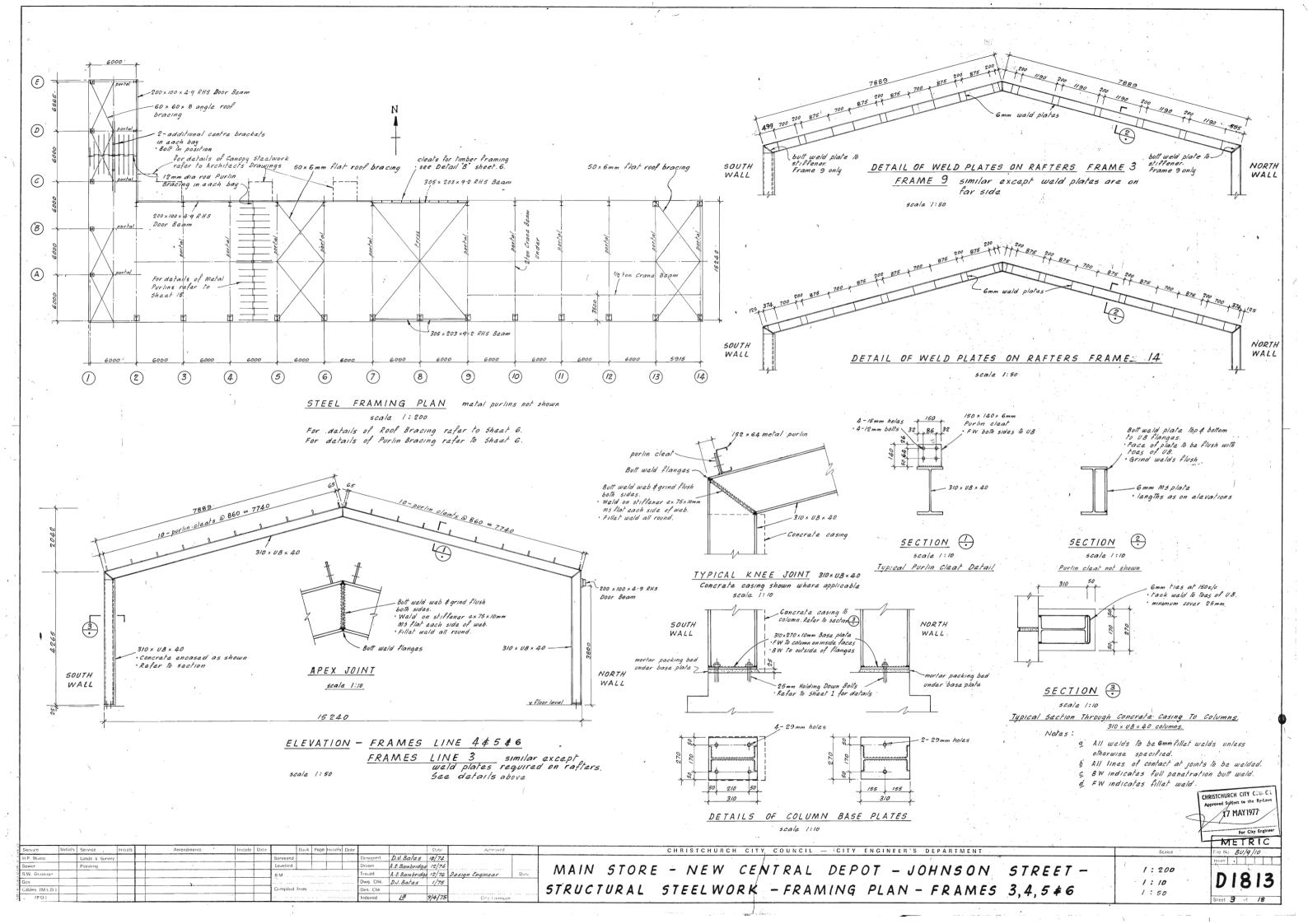


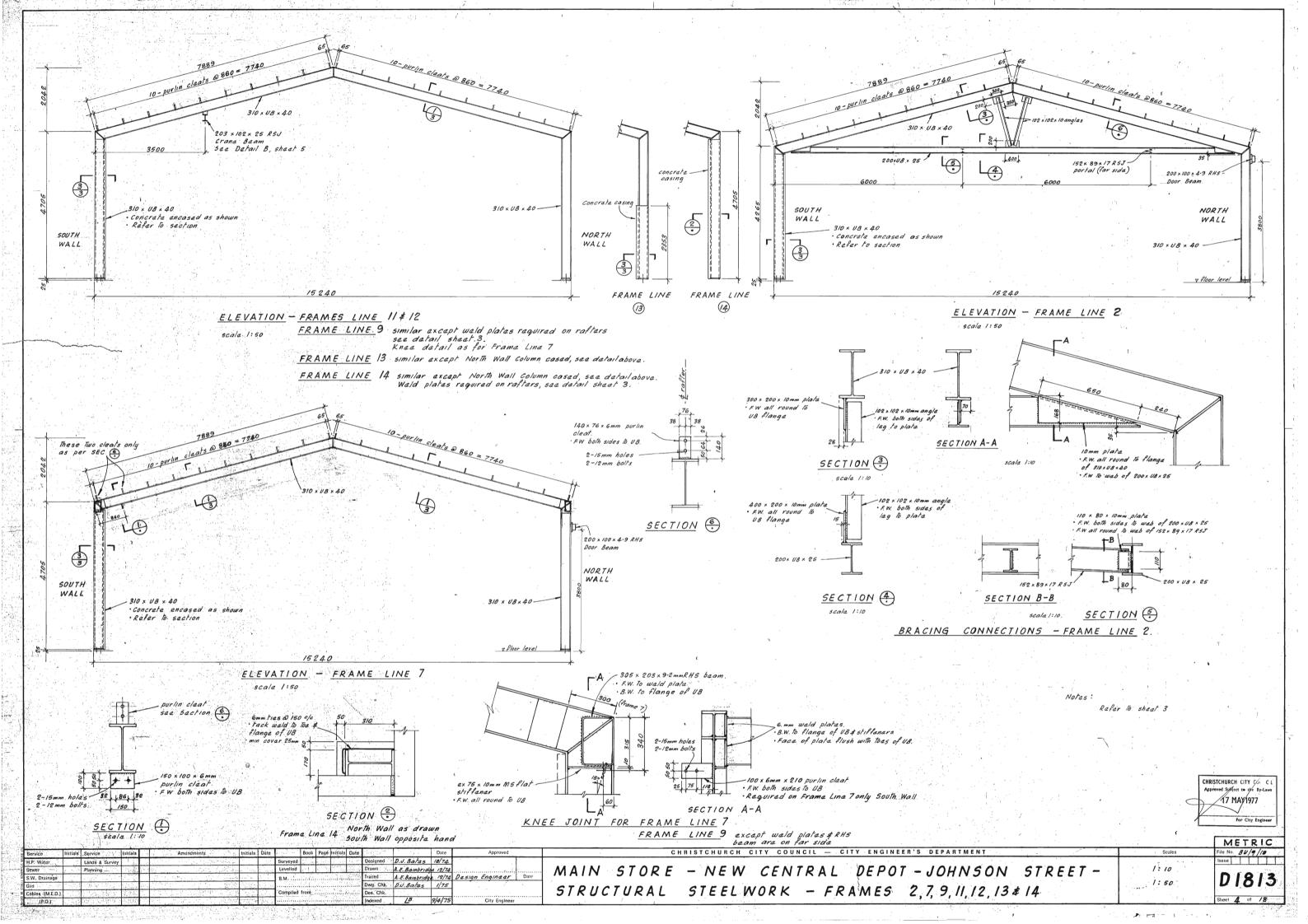


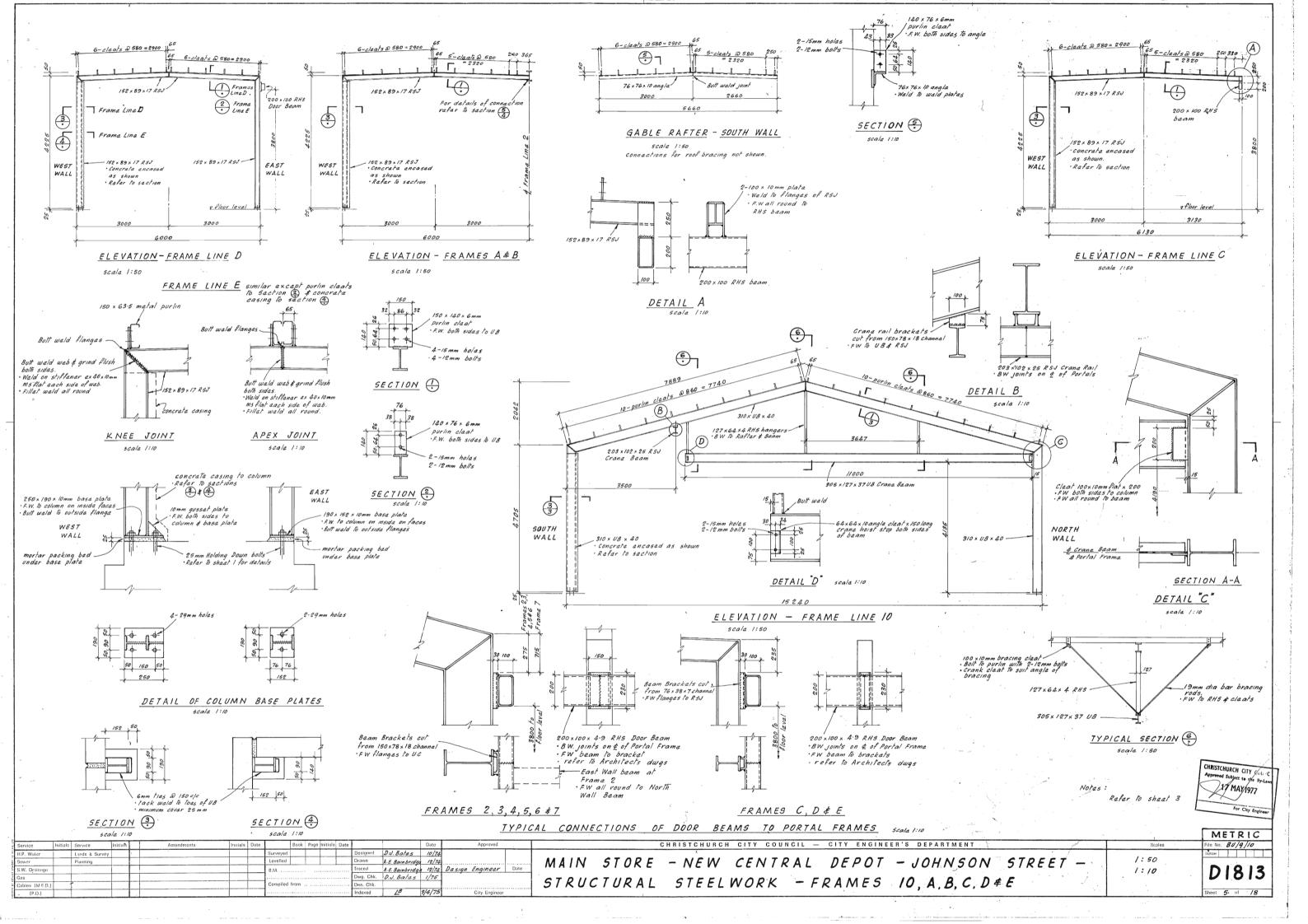


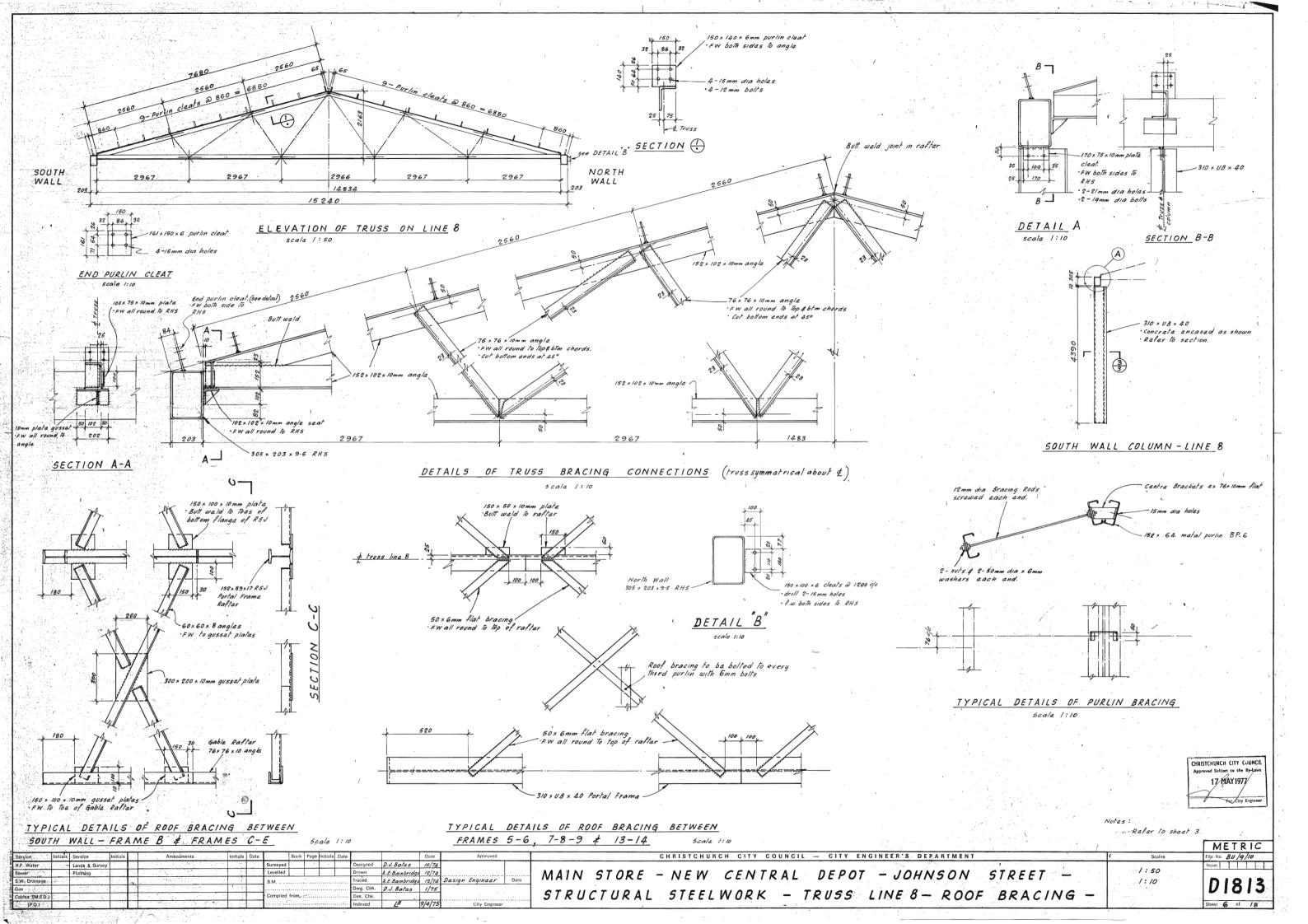


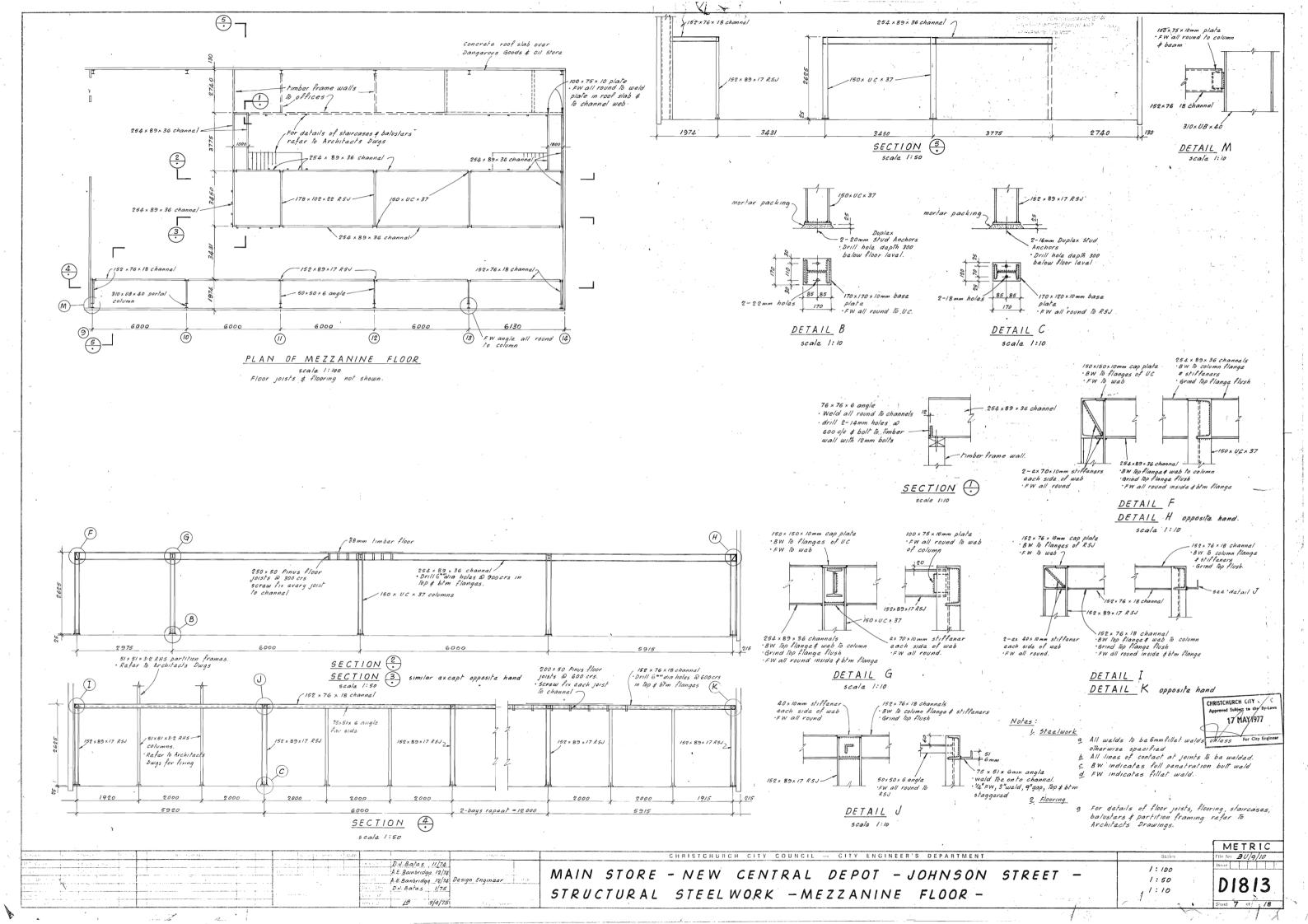


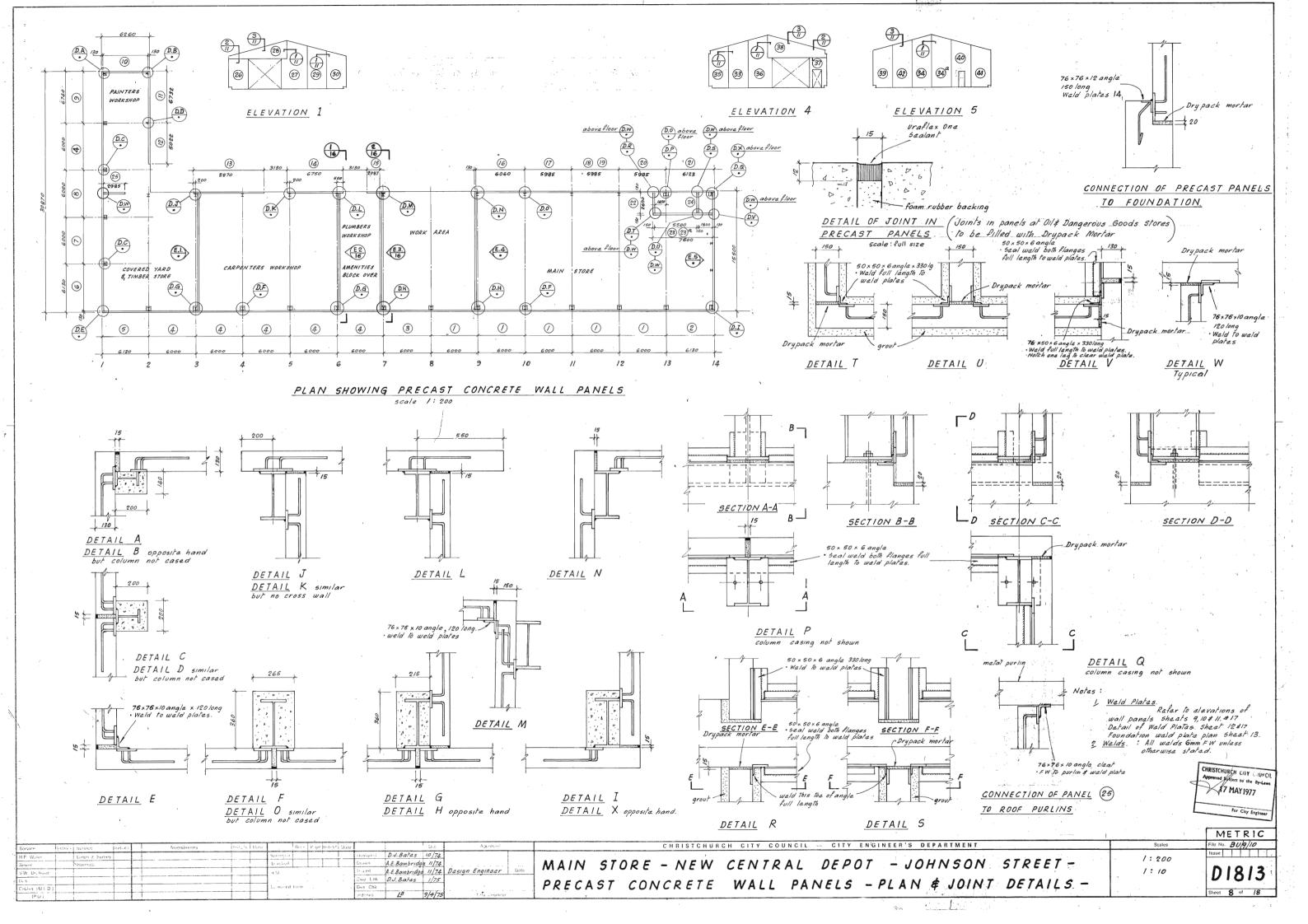


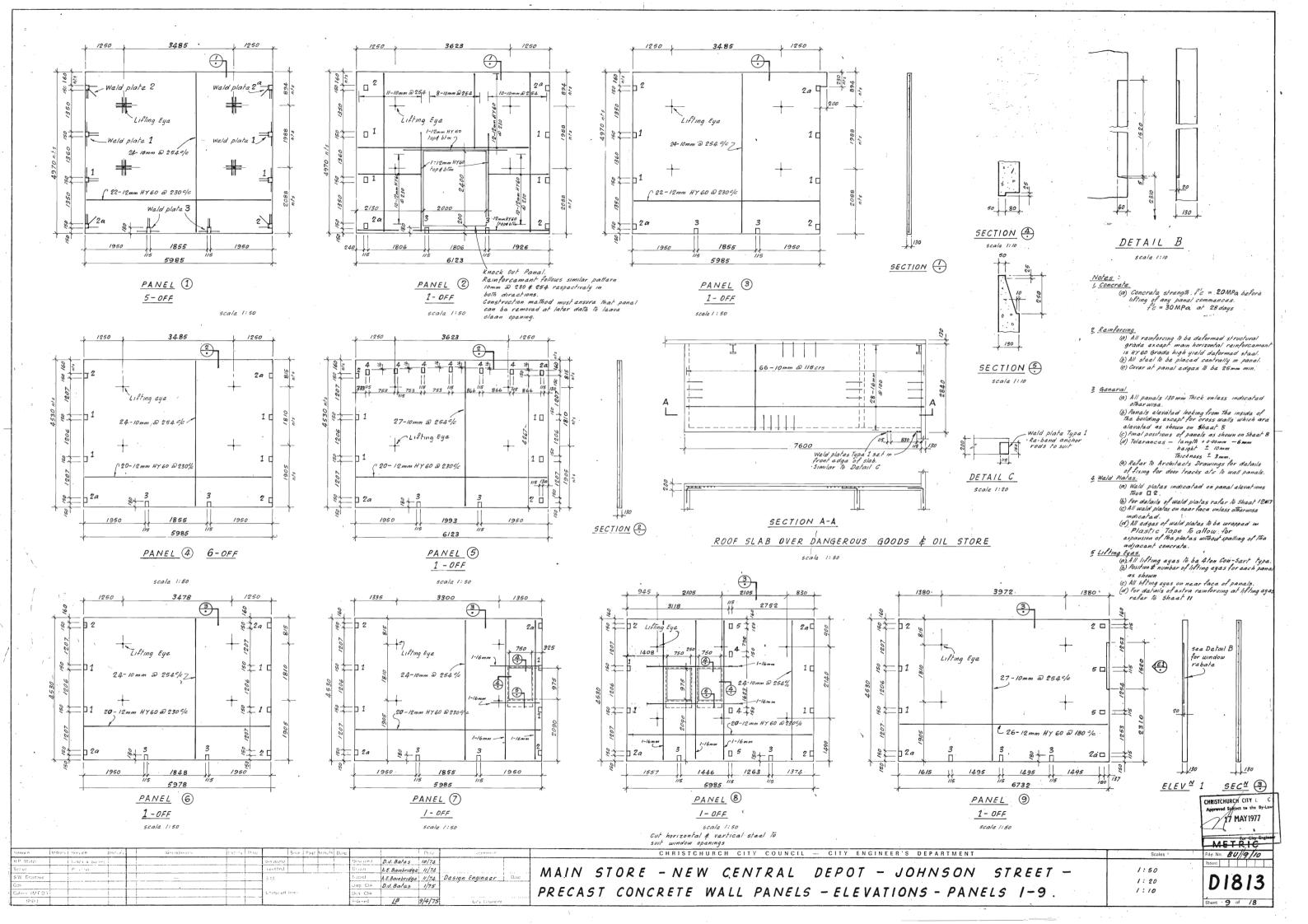


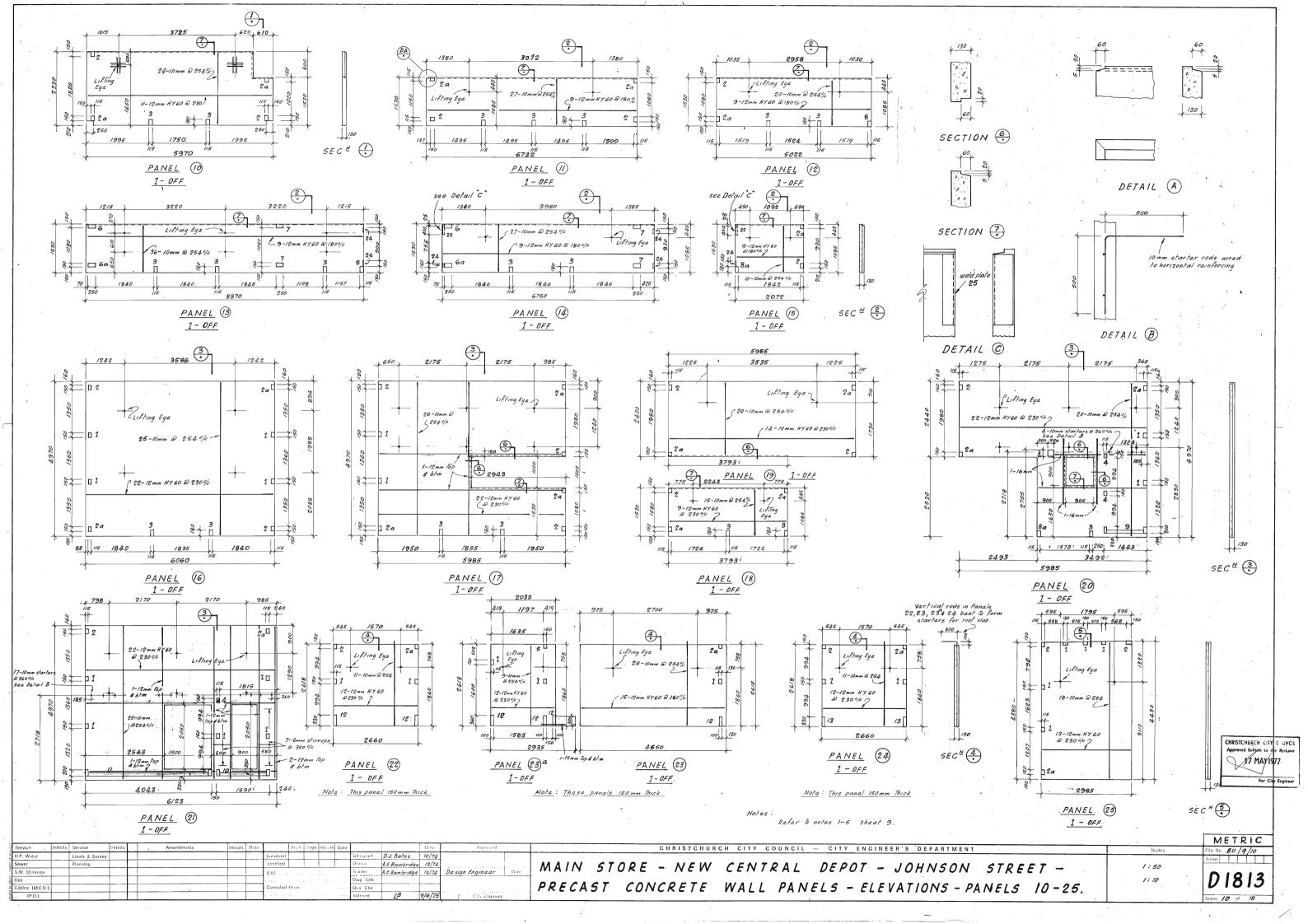


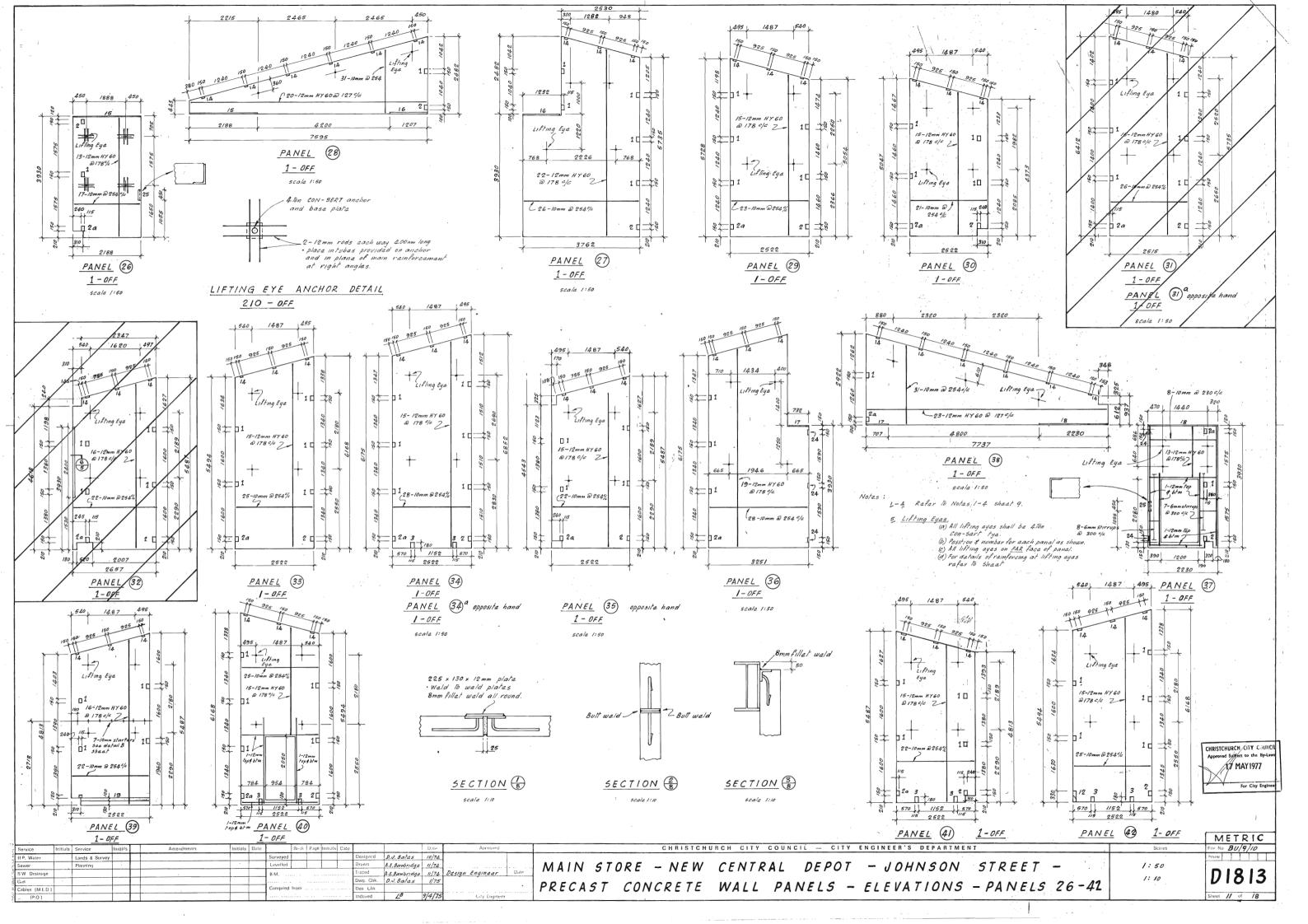


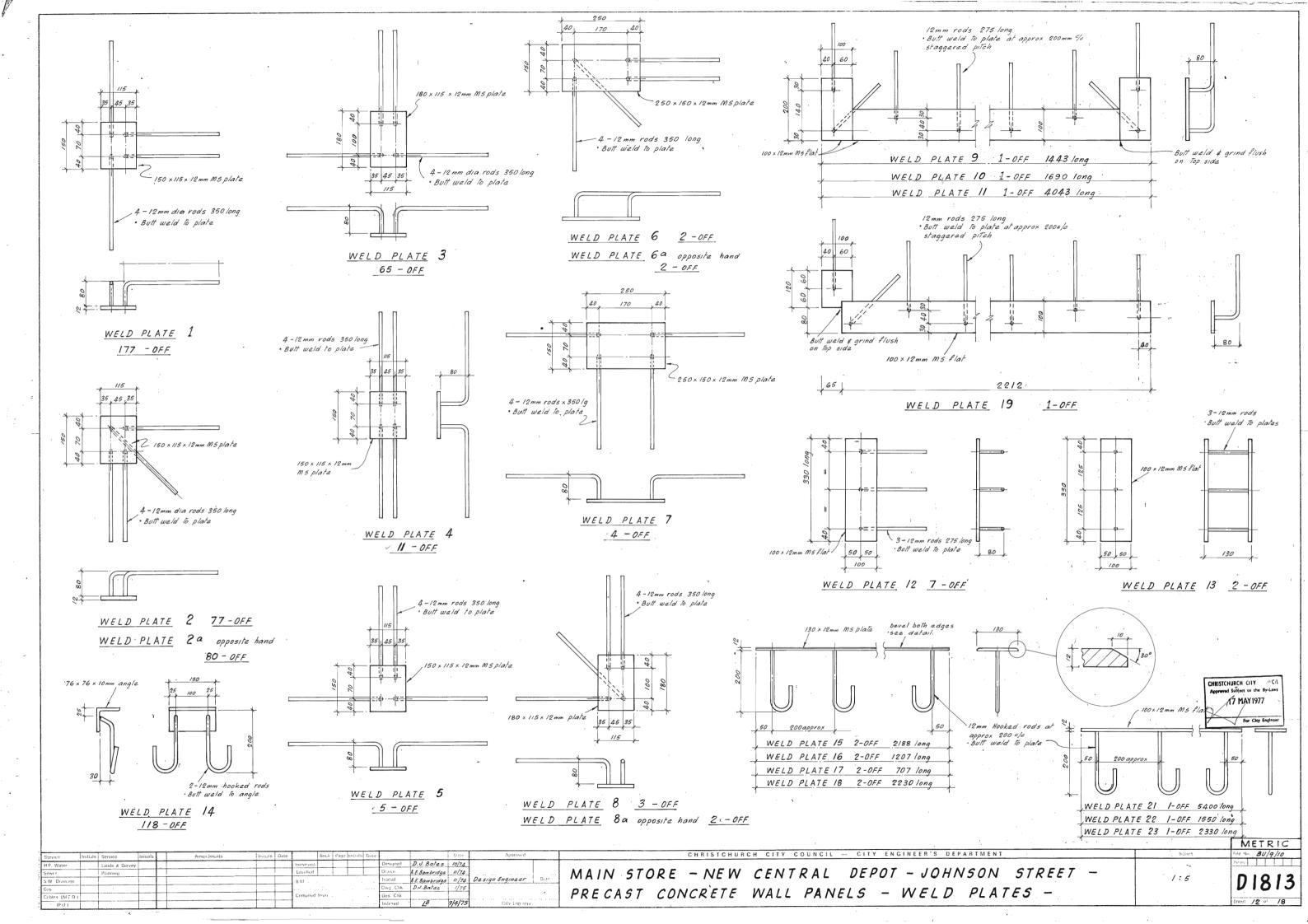


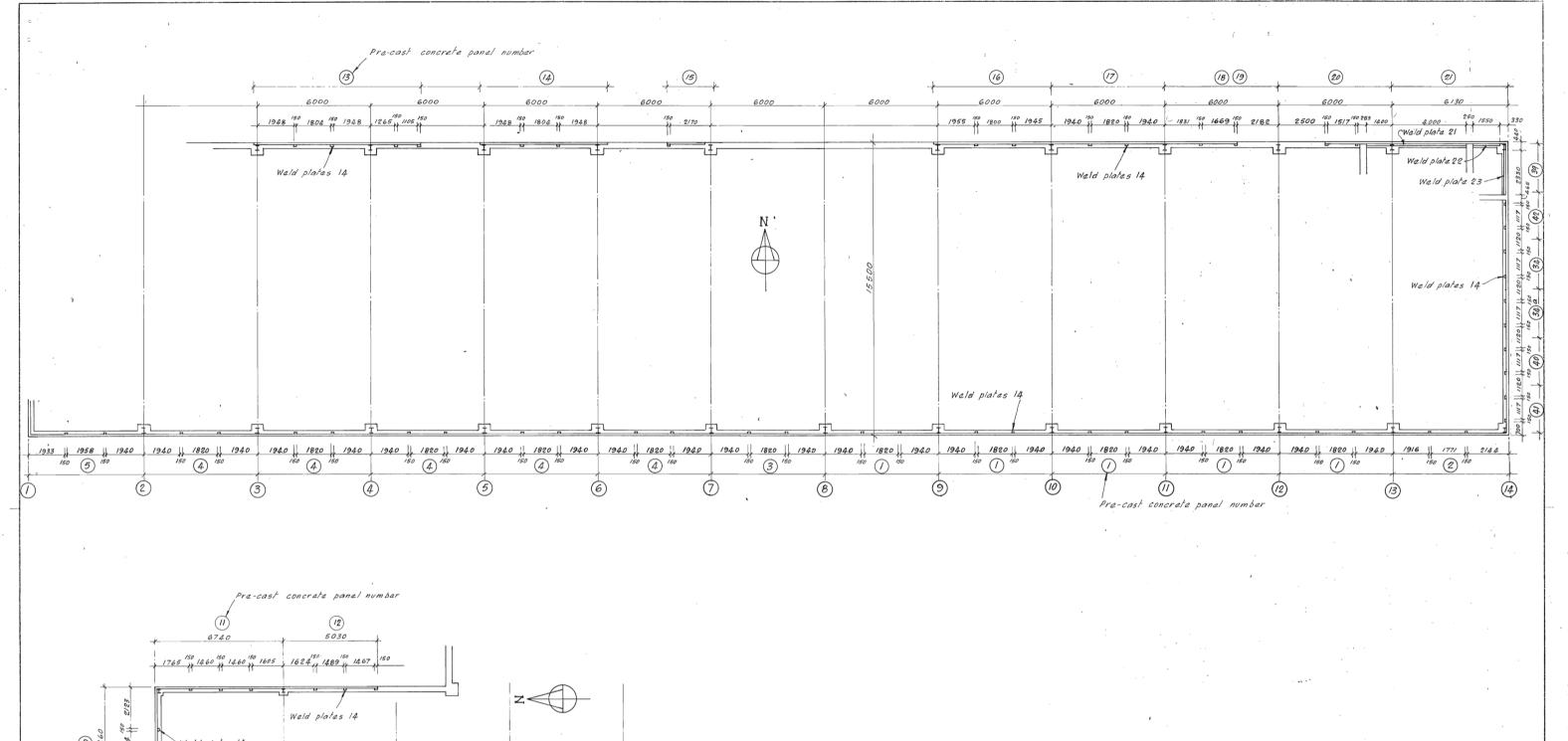


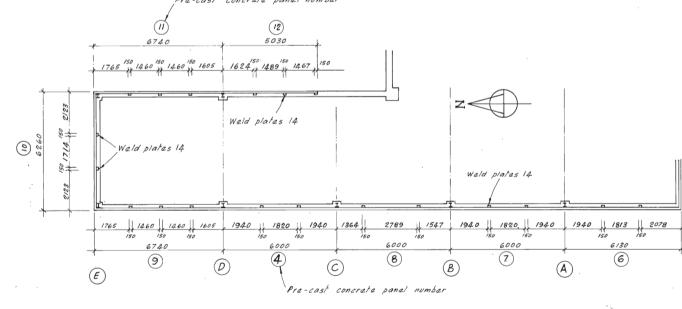












CHRISTCHURCH CITY . . . C Approved Subject to the By-Lav 17 MAY 1977 For City Engine

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Court .	I F Jacobse			1000 00.	Drawn A.E. Bainbridga 12/7	4	MAIN STORE - NEW CENTRAL DEPOT - JOHNSON STREET -	
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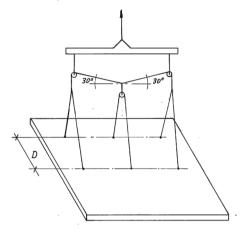
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1:100

LIFTING PROCEEDURES FOR PRE-CAST CONCRETE PANELS

2 × / RIGGING

To be used for PANELS (10) (1) (12) (14) (15) (18) (19) (22) (23) (23) (24) (25)



3×2 RIGGING

To be used for

PANELS (8) (13) (17) (20) (21)

A.E. Bainbridge 1/75

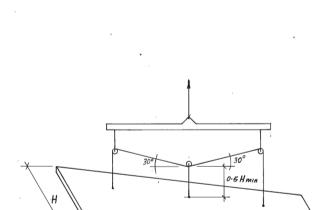
A.E. Bainbridga 1/75 Dasign Enginaar

I Cables for lifting slings shall be long enough to provide at least 60 degree angle from the plane of the panel of mitted lift from the horizontal 2 All details of proposed rigging \$ lifting equipment shall be discussed with the Engineer before lifting

2 x 2 RIGGING

To be used for

PANELS (1234567962627 2930 33 34 35 36 37 39 40 41 42 43 44 45 46



3 x / RIGGING

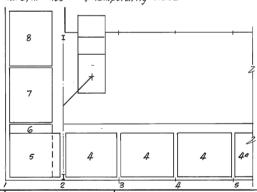
To be used for PANELS



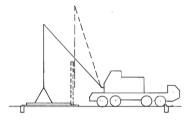
Construction Procedure.

Outling only, refer to drawings \$
specification for details of each operation

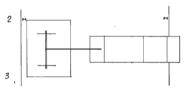
- 1, Pour all foundation beams.
- 2. Place hardfill for all floors & compact.
- 3. Pour floor in Paintars Workshop \$ batwaan Frame lines 1-2 in covared Yard. Pour floor to the south of the construction joint shown on shart I and adjacant to the south wall
- 4. Place formwork for and pour West wall tilt up panals on the concrate floor adjacant to Their final vartical positions.
- 5. Similarly place formwork and pour south wall tilt-up panals adjacent to Their final positions. Wall panal & stack cast on panal 6
- 6 Assambla Portal Frames outside building area and place in position for lifting.
- 7 Prapara casting bads outside building and stack cast Wall Units 26 - 46
- 8 Eract Frame Line 2 Portal with crane on the hardfill thus - # tamporarily braca



9 Eract wall unit 4) batwaan Frama Linas 2-3 and wald to Portal lag and foundation, bracing the other and of the panel.



30 T Crana 30'-0" Jib

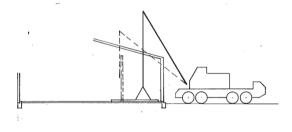


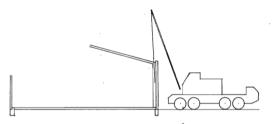
- 10 Move crane to next bay Frame Lines 3-4
- 11 Eract Portal Frame Line 3 and wald to wall unit 4 already eracted. Temporary brace north column of Portal.
- 12 Eract wall unit 4, batwaan Frames Lina 3-4 and wald to Portal lag, bracing the free and of the panal.
- 13 Place cross wall units on Frame Line 3 with crane still operating off hardfill.
- 14 Proceed eracting Portals and south wall panals in The sama saquanca, complating cross walls before eracting the next Portal Frama;

ia: Portal Frama Lina 4 Wall unit 4 , Frama Lina 4-5 Portal Frame Line 5 Wall unit 4a, Frame Line 5-6 Portal Frame Line 6 Wall unit 4, Frame Line 6-7 Cross wall units, Frame 6 Portal Frame Line 7 atc,

- 15 Return to the West and of the building, and follow a similar procedure to erect the West wall units and Portal Frames linas A, B, C, D # E.
- 16 Pour ramaining floors.
- 17 Place formwork for and pour all remaining wall units on The concrata floor adjacant to Their final positions.
- 18 EiTher form and pour wall units 22 24 outside on casting bads or on floor adjacant to South Wall.

19 Eract ramaining wall units with the crana outside the building.





Panals slawad to bring tham from insida the portals in the vertical position to thair final position outsida.

Complete fixing of purlins & wind bracing & roofing.

All panels to be lifted by filting about bottom edge & there after to remain in vertical position. Panels can not be lifted or handled in the flat position without using strongback frames, — details of frames to be submitted for approval by the Engineer prior to flat lifting

1:200

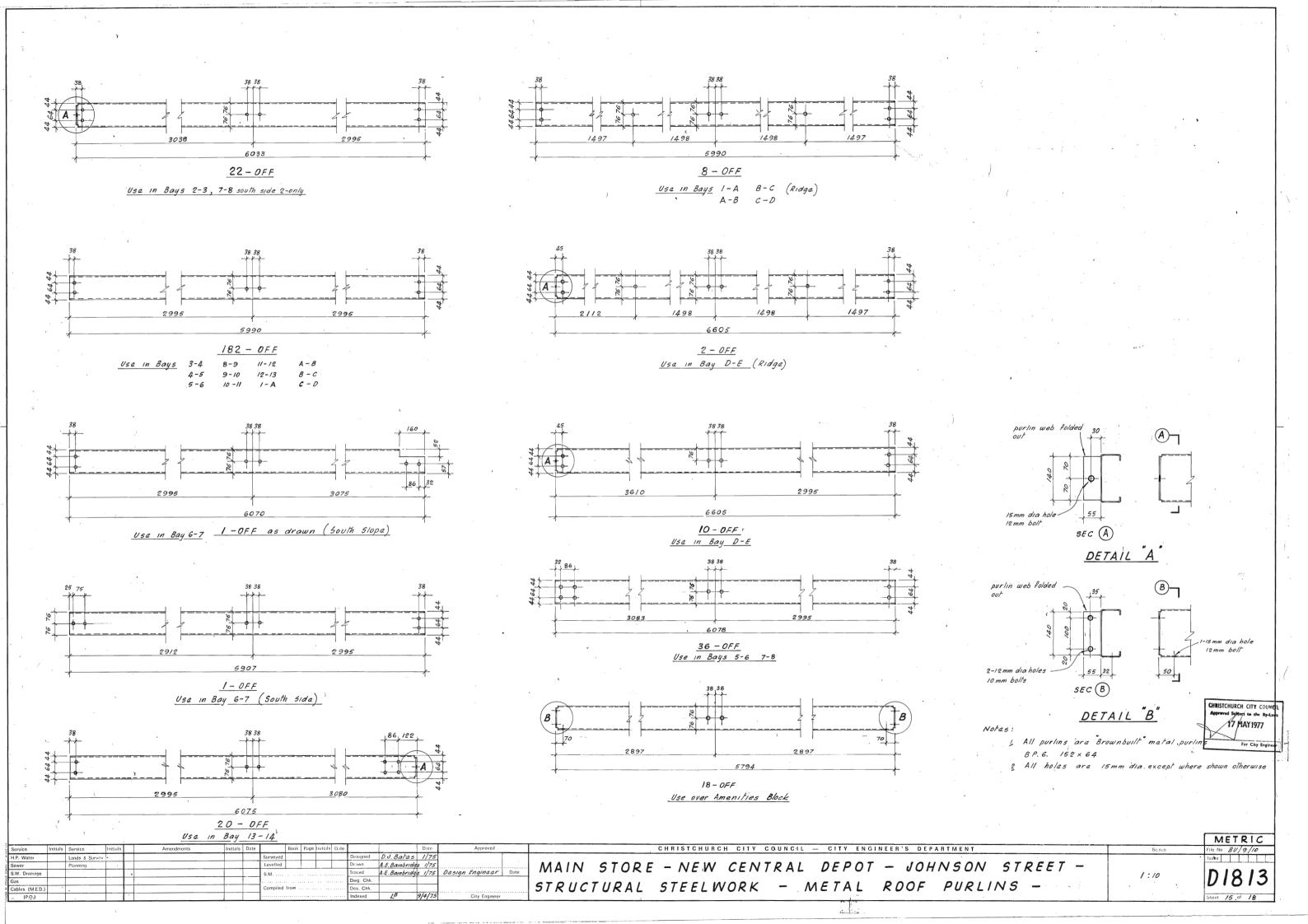
CHRISTCHURCH CITY . C 17 MAY 1977

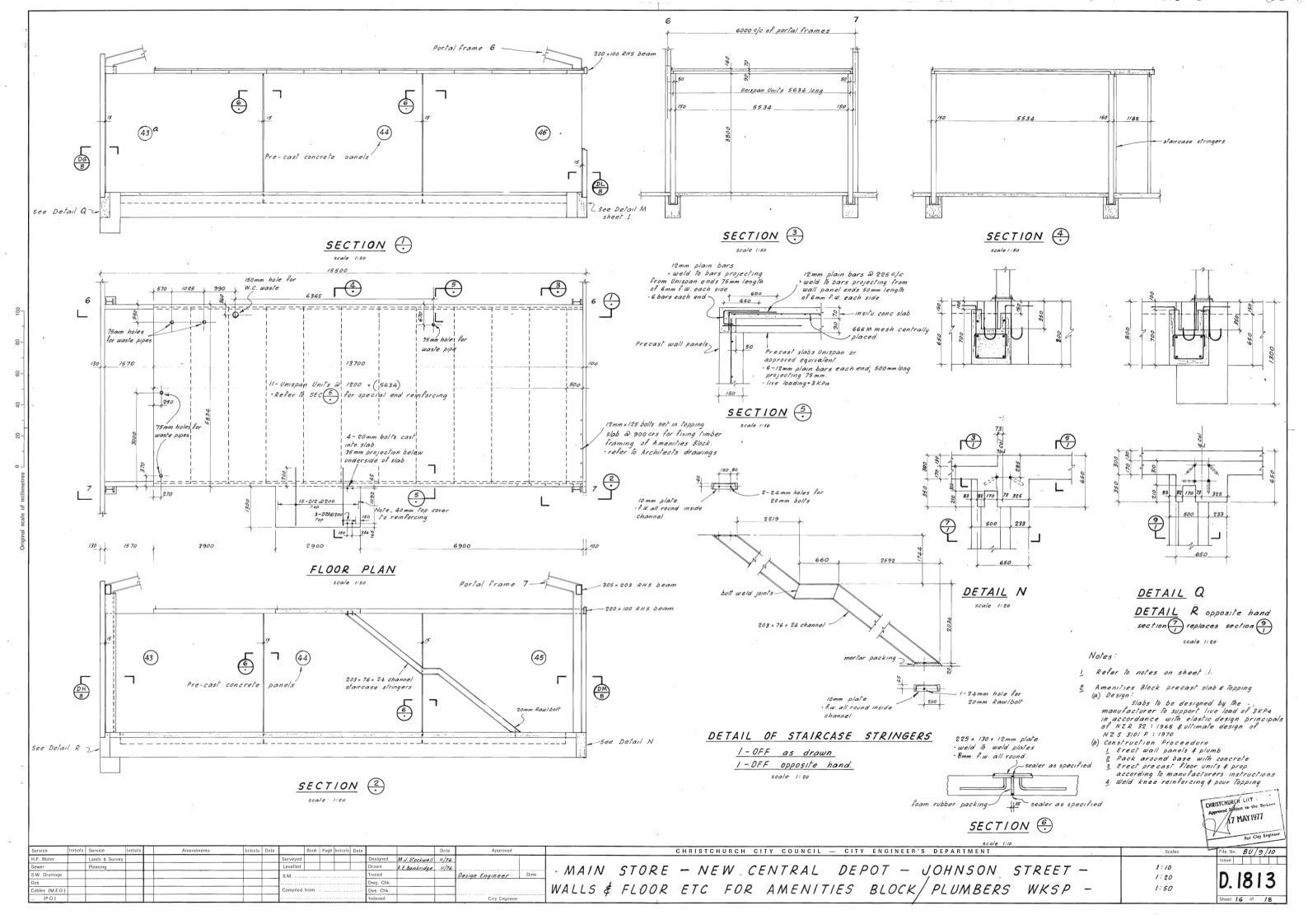
CHRISTCHURCH CITY COUNCIL — CITY ENGINEER'S DEPARTMENT

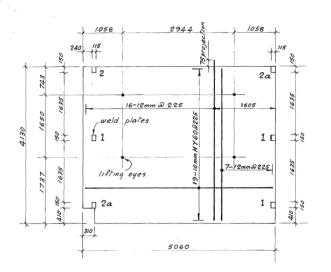
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MAIN STORE - NEW CENTRAL DEPOT - JOHNSON STREET -CONSTRUCTION PROCEDURE





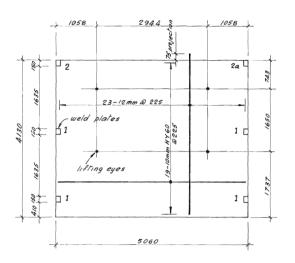


PANEL (43)

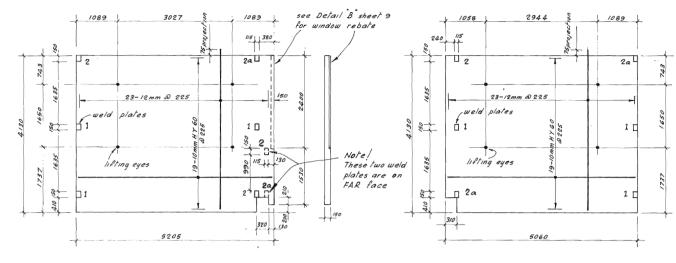
1-OFF

PANEL (43)

1-OFF

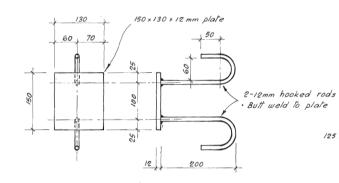


<u>PANEL</u> (44) 2 - OFF



<u>PANEL</u> 45 1 - 0FF <u>PANEL</u> 46 1 - OFF

Note | Panels 43 to 46 inclusive are 150 mm thick



ked rods
To plate

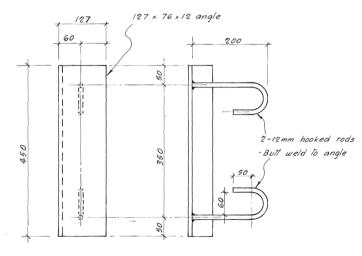
125 × 125 × 10mm plate

10mm rod
butt weld to plate

WELD PLATE 26
4-OFF

WELD PLATE 24 10-OFF

scale 1:5



hardfill 2 | 1-16nm |

TYPICAL SECTION THROUGH VEHICLE
RAMPS AT DOORWAYS

· For dimensions of Ramps refer to Architects drawings.

scale 1:20

Notes.
1 All weld plates are on NEAR face except
where shown otherwise on Panel 45
2 All Lifting Eyes are on FAR face.

1:50

1:5

3 Refer to Notes on sheet 9.

WELD PLATE 25 4-OFF

scale 1:5

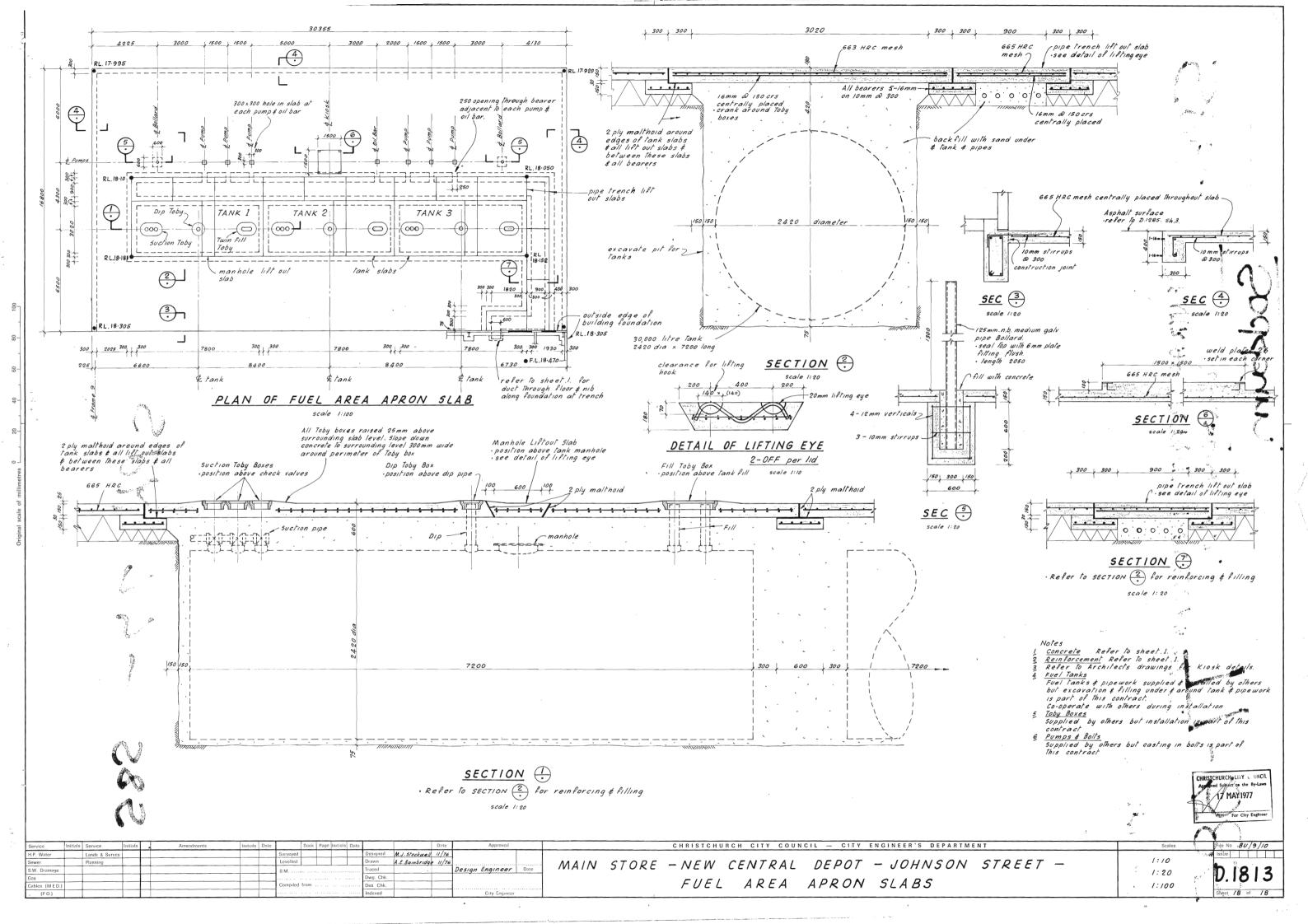
ervice	Initials	Service	Initials	Amendments	Initials	Date		Book	Page	Initials	Date			Date		Approved	
.P. Water		Lands & Survey					Surveyed					Designed	M.J. Stockwell	11/76			
ewer		Planning					Levelled					Drawn	A.E. Bainbridge	11/76			
.W. Drainage							в м					Traced			Design	Engineer	Date
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ables (M.E.D.)							Compiled	from .				Des. Chk					
(P.O.)												Indexed				City Engineer	

MAIN STORE - NEW CENTRAL DEPOT - JOHNSON STREET
PRECAST CONCRETE WALL PANELS 43 - 46-WELD PLATES 24-26

CHRISTCHURCH CITY COUNCIL
Approved Subject to the By-Laws
17 / 1AY 1977

For City Engineer

D. 1813



Appendix C

CERA DEE Summary Data

35% #### %NBS from IEP below 35%

Assessed %NBS before: Assessed %NBS after:

3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Alignment of floors within 20% of H 0.7 0.8 Alignment of floors not within 20% of H 0.4 0.7	IEP.
Period (from above): 1.00 2.00 2.00 3.00 3.00	
Period (from above):	
Period (from above): (SNBS)spont from Fig. 2. and Assistant public buildings, to the code of the day: pre-1965 = 1.25; 1965-1976, Zone A. F. 1.23; 1965-1976, Zone B. P. 1.23; 1965-1976, Zone B. 1.23; 1965-19	ee.
Note: 1 for specifically design public buildings, to the code of the day: pre-1965 = 1.26: 1965-1976, Zone A = 1.33: 1966-1976, Zone B = 1.2: all else 1.0 Note: 2 for Roulidings designed between 1976-1984, use 1.2 Note: 3 for buildings designed between 1976-1984, use 1.2 Note: 3 for buildings designed between 1976-1984 use 1.2 Note: 3 for buildings designed between 1976-1984 use 1.2 Abong	
Note 3: for RCD buildings designed prior to 1935 use 0.8, except in Wellindon (1.0) Real Note 3: for buildings designed prior to 1935 use 0.8, except in Wellindon (1.0)	
Page Pault Scaling Factor Pault Scaling Factor Page Pault Scaling Factor Pault Scaling Factor Page P	
2.2 Near Fault Scaling Factor Near Fault scaling factor (1/N(T,D), Factor A: along acre acre along factor Assarch (1/N(T,D), Factor A: along acre acre acre along factor, Factor B: along acre acre acre acre acre acre acre acre	
Near Fault scaling factor (1/N(T,D), Factor A: #BDIV/0! #BDIV 2.3 Hazard Scaling Factor #BDIV/0! #BDIV 2.4 Return Period Scaling Factor #BUIding Importance level (from above): #BUIding Importance level (f	
Near Fault scaling factor (1/N(T,D), Factor A:	
2.3 Hazard Scaling Factor Hazard factor Z for site from AS1170.5, Table 3.3: Z1982, from MZS42031992 Hazard scaling factor B: #DIN 2.4 Return Period Scaling Factor Building Importance level (from above): Return Period Scaling factor Factor C: 2.5 Ductility Scaling Factor Assessed ductility (less than max in Table 3.2) Ductility Scaling Factor: =1 from 1976 onwards; or =kg, if pre-1976, from Table 3.3: Ductility Scaling Factor. Factor D: 1.00 1.1.6 2.6 Structural Performance Scaling Factor: Structural Performance Scaling Factor Factor E: #DIN/0! #DIN 2.7 Baseline %NBS, (NBS%) = (%NBS) = (%NBS) = X x X X X X X X X X X X X X X X X X X	
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2.6 Structural Performance Scaling Factor: Structural Performance Scaling Factor Factor E: Structural Performance Scaling Factor Factor E: #DIV/0! #DIV. 2.7 Baseline %NBS, (NBS%)b = (%NBS)boom x A x B x C x D x E %NBSb: #DIV/0! #DIV. #DIV	
Structural Performance Scaling Factor E)
Structural Performance Scaling Factor E	
2.7 Baseline %NBS, (NBS%) = (%NBS)nom x A x B x C x D x E Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4) 3.1. Plan Irreqularity, factor A: 3.2. Vertical irregularity, Factor B: 1 3.3. Short columns, Factor C: 1 3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Alignment of floors within 20% of H Alignment of floors within 20% of H Alignment of floors not within 20% of H Alignment of floors on within 20% of H Alignment of floors not within 20% of H Alignment of floors not within 20% of H Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 Alignment of floors on within 20% of H O.7 O.8 O.9 Height difference < 2 to 4 storeys Height difference < 2 to 4 storeys Alignment of floors on within 20% of H O.7 O.8 O.9 Height difference < 2 to 4 storeys Alignment of floors on within 20% of H O.7 O.8 O.9 Height difference < 2 to 4 storeys Alignment of floors on within 20% of H O.7 O.8 O.9 O.9 O.9 O.9 O.9 O.9 O.9	(01
Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4) 3.1. Plan Irregularity, factor A: 3.2. Vertical irregularity, Factor B: 3.3. Short columns, Factor C: 3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Alignment of floors within 20% of H Alignment of floors within 20% of H O.7 O.8 Therefore, Factor D: Therefore, Factor D: 1 3.5. Site Characteristics 1 Table for selection of D1 Separation O <sep<.005h 20%="" alignment="" d2="" difference="" floors="" for="" h="" height="" ins="" o.5csep<.01h="" o.7="" o.8="" o<sep<.005h="" of="" selection="" separation="" severe="" significant="" table="" within=""> 4 storeys O.4 O.7 Height difference > 4 storeys O.4 O.7 Height difference 2 to 4 storeys Height difference < 2 storeys O.7 O.9 Height difference < 2 storeys OFF OFF OFF OFF OFF OFF OFF OFF OFF OF</sep<.005h>	0!
3.1. Plan Irregularity, factor A: 1 3.2. Vertical irregularity, Factor B: 1 3.3. Short columns, Factor C: 3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Therefore, Factor D: 7 1 3.5. Site Characteristics 1 1 3.6. Severe Significant Insert Of sport within 20% of H O.7 O.8 Alignment of floors within 20% of H O.7 O.8 Separation Separation O-sepe_005H O.5 sepe_01H O.7 Height difference > 4 storeys O-4 Height difference > 4 storeys O-7 Height difference > 4 storeys O-7 Height difference > 2 to 4 storeys Height difference < 2 to 4 storeys Height difference < 2 storeys O-7 O-9 Height difference < 2 storeys O-7 O-9 Height difference < 2 storeys O-7 O-9 O-9 Height difference < 2 storeys O-7 O-9	/0!
3.1. Plan Irregularity, factor A: 3.2. Vertical irregularity, Factor B: 3.3. Short columns, Factor C: 3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Alignment of floors within 20% of H Alignment of floors within 20% of H Alignment of floors within 20% of H O.7 Alignment of floors within 20% of H O.4 O.7 Table for Selection of D1 Separation O-sep<.005H O-sep<.01H O-sep<.005H O-sep<.01H Height difference > 4 storeys O-sep<.01H Height difference > 4 storeys O-sep<.005H O-sep<.01H Height difference > 4 storeys O-sep<.01H Height difference > 4 storeys O-sep<.01H Height difference > 4 storeys O-sep<.01H O-s	
3.2. Vertical irregularity, Factor B: 1 3.3. Short columns, Factor C: 1 3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Therefore, Factor D: 3.5. Site Characteristics 1 Table for selection of D1 Separation O-sep<005H O.7 O.8 Alignment of floors within 20% of H O.7 O.8 Separation O-sep<005H O.5 sep<01H O-5 sep<01H Alignment of floors not within 20% of H O.7 O-sep<005H O-sep<0	
3.3. Short columns, Factor C: 1 Table for selection of D1 Severe Significant Ins Separation O-sep<.055H O-56=p<.01H Alignment of floors within 20% of H Alignment of floors not within 20% of H O.7 O.8 Alignment of floors within 20% of H O.7 O.8 Separation O-sep<.059H O-56=p<.01H O-7 O-8 Separation O-sep<.059H O-56=p<.01H O-7 O-8 Height difference 4 storeys Height difference 2 to 4 storeys Height difference < 2 to 4 storeys Height difference < 2 storeys 1	
3.4. Pounding potential Pounding effect D1, from Table to right Height Difference effect D2, from Table to right Therefore, Factor D: Table for Selection of D2 Separation Separation O <sep<.005h 20%="" alignment="" d2="" floors="" for="" h="" o.5<sep<.01h="" o.7="" o<sep<.005h="" of="" oots<ep="" out="" selection="" separation="" table="" within="">.005<sep<.01h difference="" height=""> 4 storeys Height difference 2 to 4 storeys Height difference < 2 to 4 storeys Height difference < 2 storeys Table for Selection of D2 Separation O<sep<.005h oots<ep="">.005<sep<.01h oots<ep="">.07 Oots<ep>.07 Height difference < 2 to 4 storeys Height difference < 2 to 4 storeys Height difference < 2 storeys Table for Selection of D2 Severe Significant Institute of the control of the control</ep></sep<.01h></sep<.005h></sep<.01h></sep<.005h>	
Alignment of floors within 20% of H	gnificant/none Sep>.01H
Alignment of floors not within 20% of H 0.4 0.7 Alignment of floors not within 20% of H 0.4 0.7 Therefore, Factor D: 0 3.5. Site Characteristics 1 Alignment of floors not within 20% of H 0.4 0.7 Table for Selection of D2 Severe Significant Institution of Separation 0.4 0.7 Height difference > 4 storeys 0.4 0.7 Height difference 2 to 4 storeys 1.7 Height difference < 2 to 4 storeys 1.7 Height difference < 2 storeys 1.7 Height difference < 2 storeys 1.7 Alignment of floors not within 20% of H 0.4 O.7 Table for Selection of D2 Severe Significant Institution of H 0.4 O.7 Height difference > 4 storeys 1.7 Height difference < 2 to 4 storeys 1.7 Height difference < 2 storeys 1.7 Height differenc	1
Separation O-sep005H .005-sep01H	0.8
Height difference > 4 storeys	gnificant/none
Height difference > 4 storeys	Sep>.01H
Height difference < 2 storeys 1 1	1
	1
3.6. Other factors, Factor F For ≤ 3 storeys, max value = 2.5, otherwise max valule = 1.5, no minimum	33
Rationale for choice of F factor, if not 1	
Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)	
Detail Critical Structural Weakriesses. (refer to DEE Procedure Section 6) Refer also section 6.3.1 of DEE for discussion of F factor modification for other critical structural weaknes	es
3.7. Overall Performance Achievement ratio (PAR) 0.00 0.0)
- July 1	
4.3 PAR x (%NBS)b: PAR x Baselline %NBS: #DIV/0! #DIV	/01
4.4 Percentage New Building Standard (%NBS), (before)	.0!

Appendix D

Previous Reports and Assessments

city // care

Project			Job No/File	Ref		
Description	BU 1140	-001	Prepared b	y		
6m7			Date	11	Sheet No	of
	Site Instruction:	Memo:	Meeting:	File Note:	Variation / Detail	: 🗌
			1/2	C	etycane 10	
			Nish)		Log 0	
	Buil	diz Serv				
			sq = lm	3	3	
	/x////	,	WC -4	<u>8</u>		1
eiling par	nd Point	<u> </u>	\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	Sign Shop Norkroom	Print Office	,
logged and	y Store	}	bluk /	Workroom	5.77	7
<u> </u>		1			3"-1 6-3-	
11e.				rake	e & fill firewall a	is cracles.
1200 x 1200	1514		9	7		
= 17116)					Eiling Space	
					temp office.	₹ . ₹ .∠2
	~		4//	4	y	12.5
						30 m².
			*@	a Vilis	૦(ભાર ,	(1 , //-)
				talet	upstairs	(temp office)
			Men			2
			hill			1 2
	I 24m	1			MINNE	
				- W		
Approved	Client Date	1 1		Contractor Date /	1	
Distributio		Contractor:	Site Copy: Er		b-Contractor: Jo	b File:





Ph

Scope of Works & Cost Estimate Form For EQ Damage

 Building Name
 Milton st Depot-Tradesmen Workshop

 Building BU No.
 BU 1141-001 EQC
 Date
 4/05/2011

 CCL Fee
 16.66%

 Inspection Team
 CCL Scott Titheridge
 Page Date Visited
 11/04/2011

 CL Scott Titheridge
 Site Contact
 Mike Okey

DAMAGED AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	R	ate (\$)	Rate Including fee	CCL	Cost ncluded CCL Fee
Tradesmen Work Shop									
Female Toilet		Ceiling Cracks - General any substrate - Rake, RTV and touch up.	Lm	2	\$	12.00	\$	14	\$ 28
Paint Store	Α	Re Screw Popped Nails	m2	2	\$	50.00	\$	58	\$ 117
	Α	Ceilings - Paint - Repaint -2 coats	m2	36	\$	17.00	\$	20	\$ 714
	В	Wall - Cracks - Plasterboard - Rake & no more gaps	Lm	3	\$	10.00	\$	12	\$ 35
		Scaffolding mobil	d	5	\$	25.00	\$	29	\$ 146
		Stop ceiling	M2	3	\$	15.00	\$	17	\$ 52
Joinery Wok Room	С	Re Place Damaged Ceiling Tiles	day	3	\$	480.00	\$	560	\$ 1,680
		Lift - Scissor lift 6m	day	3	\$	100.00	\$	117	\$ 350
		New Replacement Tiles	M2	15	\$	40.00	\$	47	\$ 700
		Lift - Scissor lift 6m transport	Bothw ays	1	\$	90.00	\$	105	\$ 105
	D+E	Repair cracks Concrete floor blow out and Grind andEpoxy	Lm	39	\$	14.00	\$	16	\$ 637
Sign Shop Office	F	Wall - Cracks - Pre cast panels Structurally repaired using Epozy injection	Lm	1	\$	197.98	\$	231	\$ 231
		Walls - Paint - Repaint	m2	3.7	\$	12.00	\$	14	\$ 52
	G	Wall - Cracks - Plasterboard - Rake & Stop	Lm	2	\$	12.00	\$	14	\$ 28
		Walls - Paint - Repaint	m2	9	\$	12.00	\$	14	\$ 126
	Н	Wall - Cracks - Plasterboard - Rake & Stop	Lm	4	\$	12.00	\$	14	\$ 56
	1	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	3	\$	14.50	\$	17	\$ 51
		Ceilings - Paint - Repaint -2 coats	m2	20	\$	17.00	\$	20	\$ 397
Sign Work Room	J	Wall Cracks - General any substrate - Rake, RTV and touch up.	Lm	20	\$	10.00	\$	12	\$ 233
		Walls - Paint - Repaint	m2	2	\$	12.00	\$	14	\$ 28
		Scaffolding mobil	Day	2	\$	25.00	\$	29	\$ 58
Print Shop	k	Wall - Cracks - Plasterboard - Rake & Stop	Lm	5	\$	12.00	\$	14	\$ 70
		Walls - Paint - Repaint	m2	14	\$	12.00	\$	14	\$ 196
Sign Work Shop Floor		Blow out , install 10mm dia PF rod and fill with Seks Grey RTV.	Lm	15	\$	25.00	\$	29	\$ 437
Column Sign Work Shop	L	Engineers Inspection, Report and Design Brief (Provisional Sum)	PS	1	\$:	1,500.00	\$ 1,7	750	\$ 1,750
Temp Office Stair	Α	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	6	\$	14.50	\$	17	\$ 101
		Ceilings - Paint - Repaint -2 coats	m2	15.5	\$	17.00	\$	20	\$ 307
Walls Stairs	В	Wall - Cracks - Plasterboard - Rake & Stop	Lm	8.2	\$	12.00	\$	14	\$ 115
		Walls - Paint - Repaint	m2	32	\$	12.00	\$	14	\$ 448
Cylinder Cupboard	С	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	3.6	\$	14.50	\$	17	\$ 61
		Ceilings - Paint - Repaint -2 coats	m2	1.7	\$	17.00	\$	20	\$ 34
		Wall - Cracks - Plasterboard - Rake & no more gaps	Lm	2.5	\$	10.00	\$	12	29
		Walls - Paint - Repaint	m2	9.2	\$	12.00	\$	14	129
Store Room	D	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	11	\$	14.50		17	186
		Ceilings - Paint - Repaint -2 coats	m2	19	\$	17.00	\$	20	\$ 377

DAMAGED AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	R	ate (\$)	Inc	Rate luding CCL fee		Cost ncluded CCL Fee
, ,		 Wall - Cracks - Plasterboard - Rake & Stop	Lm	1.4	\$	12.00	\$	14	-	20
		Walls - Paint - Repaint	m2	22.5	\$	12.00	_	14	-	315
		Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90	_	38	<u> </u>	154
Mens Toilet	Е	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	10.2	\$	14.50	\$	17	\$	173
		Ceilings - Paint - Repaint -2 coats	m2	20	\$	17.00	\$	20	\$	397
Ladies Toilet	F	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	3.8	\$	14.50	_	17		64
		Ceilings - Paint - Repaint -2 coats	m2	3	\$	17.00	_	20	\$	59
Store 2	G	Wall - Cracks - Plasterboard - Rake & Stop	Lm	9.6	\$	12.00	_	14	\$	134
		Walls - Paint - Repaint	m2	30	\$	12.00	\$	14	\$	420
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90	\$	38	\$	77
Office	Н	Ceiling - Cracks - Junctions & Negative Details -	Lm	10	\$	5.50	\$	6	\$	64
		RTV Fill					Ť		Ľ	
		Ceilings - Paint - Repaint -2 coats	m2	2	\$	17.00	\$	20	\$	40
		Wall - Cracks - Plasterboard - Rake & Stop	Lm	5	\$	12.00	\$	14	<u> </u>	70
		Walls - Paint - Repaint	m2	44	\$	12.00	_	14		616
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90	\$	38	\$	77
D (O		Popped Screws/Nails Walls	Per	12	\$	4.00	\$	5	\$	56
Roof Space Fire Walls	I	Ceiling - Cracks - Plasterboard - Rake, Stop &	Lm	30	\$	24.50	\$	29	\$	857
Fire Hose	J	Touchup Paint Re Fix Back to wall	Hr	0.5	\$	39.32	\$	46	\$	23
Tradesmens Store	_	Wall Cracks - General any substrate - Rake, RTV	1111	0.5		33.34		40		
Room	K	and touch up.	Lm	7.8	\$	10.00	\$	12	\$	91
		Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90	\$	38	\$	154
		Mobil Scaffold	Day	2	\$	25.00	\$	29	\$	58
Floor Repair to Floor										
at door		Grind sand cerment	Lm	2.3	\$	39.00	\$	45	\$	105
Outside Duitsie	^	Wall Cracks - General any substrate - Rake, RTV	1	2	,	10.00	<u>,</u>	42	,	22
Outside Building	Α	and touch up.	Lm	2	\$	10.00	\$	12	\$	23
	В	Wall - Rake and repoint block walls	m2	1.5	\$	40.00	\$	47	\$	70
		Walls - Paint - Repaint	m2	3	\$	12.00	\$	14	\$	42
	С	Wall Cracks - General any substrate - Rake, RTV	Lm	0.5	\$	10.00	\$	12	\$	6
	ر	and touch up.	LIII	0.5	Ş	10.00	ጉ	12	Ą	U
	D	Wall - Rake and repoint block walls	m2	1.5	\$	40.00	\$	47	\$	70
		Walls - Paint - Repaint	m2	1.5	\$	12.00	\$	14	\$	21
		Walls - Paint - Repaint	m2	3	\$	12.00	\$	14		42
	Е	Window Frame - Paint -Repaint	m2	40	\$	20.50	\$	24	\$	957
Refer to J Sign Shop	F	Wall - Cracks - Pre cast panels Structurally	Lm	4.3	\$	197.98	\$	231	\$	993
recici to o digit dilop		repaired using Epozy injection					Ť		Ľ	
		Walls - Paint - Repaint	m2	26.2	\$	12.00	\$	14	\$	367
	G	Wall - Cracks - Pre cast panels Structurally	Lm	4.5	\$	197.98	Ś	231	Ś	1,039
	•	repaired using Epozy injection					Ť			
		Walls - Paint - Repaint	m2	26.2	\$	12.00	\$	14	\$	367
	Н	Wall - Cracks - Pre cast panels Structurally	Lm	4.5	\$	197.98	\$	231	\$	1,039
		repaired using Epozy injection							,	
		Walls - Paint - Repaint	m2	26.2	\$	12.00	_	14		367
		Mobil Scaffold	Day	5	\$	25.00	_	29		146
A desire Offic		Prune trees prior to painting	unit	1	\$	300.00	Ş	350	\$	350
Admin Office		Well Coals Black I 2 2 2	1.	4.2	۾ ا	42.55	, ا		_	
Tradesmens Building	Α	Wall - Cracks - Plasterboard - Rake & Stop	Lm	12	\$	12.00	\$	14	\$	168
North Wall Entrance		Wolle Daint Done: ht	m- 2	24	<u> </u>	12.00	Ċ	4.0	<i>^</i>	222
		Walls - Paint - Repaint	m2	24	\$	12.00	_	14		336
		Popped Screws/Nails Walls	Per	6	\$	4.00	_	5 28		126
South Wall	В	Door & Frame - Paint - Repaint 2 coats Window Frame - Paint -Repaint	m2 m2	4.5 20	\$	24.00				126 478
outii wdli	D	window Frame - Pallit - Repailit	1112	20				24		4/8
West Wall under stair	С	Wall - Cracks - Plasterboard - Rake & Stop	Lm	1.9	\$	12.00	\$	14	\$	27
		Walls - Paint - Repaint	m2	29	\$	12.00	Ś	14	\$	406
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90		38	<u> </u>	77
nternal Office	D	Popped Screws/Nails Walls	Per	1	\$	4.00		5		5
		Walls Interior - paint - <= 300mm	Lm	7	\$	9.00		10		
		Wall - Cracks - Plasterboard - Rake & Stop	Lm	0.3	\$	12.00		14		4
		Walls - Paint - Repaint	m2	7	\$	12.00		14		98
Ceiling Tiles	E	Readjust Tiles	hr	1	\$	40.00		47		47
		Light cover Replace	Uint	1	\$	200.00		233		233
Hire Pool North Wall		Wall Cracks - General any substrate - Rake, RTV								
	G	•	Lm	1	\$	10.00	\$	12	\$	12
Entrance	_	and touch up.								

DAMAGED AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	R	ate (\$)	Rate Including CCL fee	Cost included CCL Fee
		Mobil Scaffold	Day	4	\$	25.00		\$ 117
		Walls - Paint - Repaint	m2	85	\$	12.00		\$ 1,190
Floor	I	Floor crack -Concrete-blow out -pf rod-RTV	Lm	11.7	\$	25.00	\$ 29	\$ 341
Store	J	Wall Cracks - General any substrate - Rake, RTV and touch up.	Lm	8.1	\$	10.00	\$ 12	\$ 94
IT Room	K	Wall - Cracks - Plasterboard - Rake & Stop	Lm	4	\$	12.00	\$ 14	\$ 56
		Walls - Paint - Repaint	m2	27	\$	12.00	\$ 14	\$ 378
	<u> </u>	Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90		\$ 154
	L	Floor crack -Concrete-blow out -pf rod-RTV Carpert-Glued -Lift -Relay	Lm Unit	6	\$	25.00 150.00	\$ 29 \$ 175	\$ 175 \$ 1,050
Foyer	М	Floor crack -Concrete-blow out -pf rod-RTV	Lm	2.9	\$	25.00	\$ 29	\$ 1,030
Toyer		Wall Cracks - General any substrate - Rake, RTV						
	N	and touch up.	Lm	7	\$	10.00	\$ 12	\$ 82
Office	0	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	1.2	\$	14.50	\$ 17	\$ 20
		Ceilings - Paint - Repaint -2 coats	m2	8.3	\$	17.00	\$ 20	\$ 165
	Р	Wall - Cracks - Plasterboard - Rake & Stop	Lm	1.4	\$	12.00	\$ 14	\$ 20
		Walls - Paint - Repaint	m2	17	\$	12.00	\$ 14	\$ 238
Toilet	Q	Labour - Handyman (Incl. Vehicle) Ceiling - Cracks - Plasterboard - Rake & Stop	h Lm	4.4	\$	32.90 14.50	\$ 38 \$ 17	\$ 154 \$ 74
Tollet	ų .	Ceilings - Paint - Repaint -2 coats	m2	5.6	\$	17.00	\$ 17	\$ 74
	R	Wall - Cracks - Plasterboard -Rake & RTV	Lm	5.6	\$	11.00	\$ 13	\$ 72
		Wall - Cracks - Plasterboard - Rake & Stop	Lm	8.3	\$	12.00	\$ 14	\$ 116
		Window Frame - Paint -Repaint	m2	22.2	\$	20.50	\$ 24	\$ 531
		Floor crack -Concrete-blow out -pf rod-RTV	Lm	1.8	\$	25.00	\$ 29	\$ 52
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90	\$ 38	\$ 77
		Vinyl-Remove-Relay New	m2	1.7	\$	100.00	\$ 117	\$ 198
Mezzanine	S	Cracks -Top-Columns	Lm	4.8	\$	20.00	\$ 23	\$ 112
Spray Shop	Т	Wall Cracks - General any substrate - Rake, RTV and touch up.	Lm	2	\$	10.00	\$ 12	\$ 23
		Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90	\$ 38	\$ 154
Fammable liquids	U	Wall Cracks - General any substrate - Rake, RTV	Lm	4.2	\$	10.00	\$ 12	\$ 49
store		and touch up.	h	2	\$	32.90	\$ 38	\$ 77
		Labour - Handyman (Incl. Vehicle) Wall Cracks - General any substrate - Rake, RTV	III	2		32.90		•
Radioactive store	V	and touch up.	Lm	4.8	\$	10.00	\$ 12	\$ 56
		Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90	\$ 38	\$ 154
Outside Building B	Α	Wall Cracks - General any substrate - Rake, RTV	Lm	7	\$	10.00	\$ 12	\$ 82
Outside building b	^	and touch up.	L'''	,	۲	10.00	γ 12	γ 62
	В	Wall - Cracks - Pre cast panels Structurally repaired using Epozy injection	Lm	1	\$	197.98	\$ 231	\$ 231
	С	Window Frame - Paint -Repaint	m2	3.2	\$	20.50		
		Mobil Scaffold	Day	2	\$	25.00	\$ 29	\$ 58
	D	Wall - Cracks - Pre cast panels Structurally	Lm	1	\$	197.98	\$ 231	\$ 231
		repaired using Epozy injection Wall - Cracks - Pre cast panels Structurally					-	-
	E	repaired using Epozy injection	Lm	1	\$	197.98	\$ 231	\$ 231
	F	Tilt Panal Joins Reseal	Lm	4.5	\$	25.00	\$ 29	\$ 131
		Prune trees prior to painting	Unit	1	\$	300.00	\$ 350	\$ 350
		Mobil Scaffold	Day	2	\$	25.00	\$ 29	\$ 58
Fleet Services Work shop Sheet D. Lube Store	Α	Ceiling - Cracks - Lath & Plaster - Rake & Stop	Lm	0.9	\$	15.50	\$ 18	\$ 16
Store		Door & Frame - Paint - Repaint 2 coats	m2	1	\$	24.00	\$ 28	\$ 28
		Mobil Scaffold	Day	2	\$	25.00	•	•
Wall East	В	Tilt Panal Joins Reseal	Lm	21.5	\$	25.00	\$ 29	\$ 627
		Labour - Handyman (Incl. Vehicle)	h	8	\$	32.90	\$ 38	\$ 307
Block Wall	С	Wall Cracks - General any substrate - Rake, RTV	Lm	3	\$	10.00	\$ 12	\$ 35
Wall West	D	and touch up. Tilt Panal Joins Reseal	Lm	1.5	\$	25.00	\$ 29	\$ 44
Mezzanine	E	Wall - Cracks - Plasterboard - Rake & Stop	Lm	2	\$	12.00		
	T	Walls - Paint - Repaint	m2	4	\$	12.00		\$ 56
Office	F	Wall - Cracks - Plasterboard - Rake & Stop	Lm	2.4	\$	12.00		\$ 34
		Walls - Paint - Repaint	m2	5	\$	12.00	\$ 14	\$ 70
Compressor room	G	Tilt Panal Joins Reseal	Lm	0.9	\$	25.00		\$ 26
	1	Walls - Paint - Repaint	m2	5	\$	12.00	\$ 14	\$ 70
Lube Bay	Н	Tilt Panal Joins Reseal	Lm	7	\$	25.00	\$ 29	\$ 204

DAMAGED AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	R	ate (\$)	Rate Including CCL fee	Cost include CCL Fe	ed
Staff Room Café	J	Wall - Cracks - Plasterboard - Rake & Stop	Lm	13.2	\$	12.00	\$ 14	\$	185
		Walls - Paint - Repaint	m2	66	\$	12.00	\$ 14		924
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90	\$ 38	\$	77
Ladies Toilet	k	Wall - Cracks - Plasterboard - Rake & Stop	Lm	1.8	\$	12.00	\$ 14	\$	25
Mana Tailat		Walls - Paint - Repaint	m2	8	\$	12.00	\$ 14 \$ 14	\$	112
Mens Toilet	L	Wall - Cracks - Plasterboard - Rake & Stop Walls - Paint - Repaint	Lm m2	7	\$	12.00 12.00	\$ 14	\$	29 98
office	М	Popped Screws/Nails Walls	Per	6	\$	4.00	\$ 5	\$	28
omee		Ceilings - Paint - Repaint -2 coats	m2	25	\$	17.00	\$ 20		496
	N	Wall - Cracks - Plasterboard - Rake & Stop	Lm	3	\$	12.00	\$ 14	\$	42
		Walls - Paint - Repaint	m2	14.5	\$	12.00	\$ 14	\$	203
		Labour - Handyman (Incl. Vehicle)	h	2	\$	32.90	\$ 38	\$	77
Upstairs office stairs	0	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	11.8	\$	14.50	\$ 17	\$	200
		Ceilings - Paint - Repaint -2 coats	m2	14.5	\$	17.00	\$ 20	\$	288
		Scaffolding assembled on site with 2 weeks hire.	m2	25	\$	15.00	\$ 17	\$	437
	Р	Wall - Cracks - Plasterboard - Rake & Stop	Lm	10	\$	12.00	\$ 14	\$	140
		Walls - Paint - Repaint	m2	65	\$	12.00	\$ 14		910
		Popped Screws/Nails Walls	Per	6	\$	4.00	\$ 5	\$	28
Office top of stairs	Q	Wall - Cracks - Plasterboard - Rake & Stop	Lm	0.6	\$	12.00	\$ 14	\$	8
		Walls - Paint - Repaint	m2	8	\$	12.00	\$ 14	•	112
Main office	R	Window Frame - Paint -Repaint	m2	10.5	\$	20.50	\$ 24	\$	251
Replace ceiling light fittings and Tile	S	Labour - Handyman (Incl. Vehicle)	h	4	\$	32.90	\$ 38	\$	154
		Ceiling - new exposed grid with mineral fibre tiles.	m2	1	\$	52.30	\$ 61	\$	61
Foyer	Т	Ceiling - Cracks - Plasterboard - Rake & Stop	Lm	1	\$	14.50	\$ 17	\$	17
		Ceilings - Paint - Repaint -2 coats	m2	10.4	\$	17.00	\$ 20	•	206
		Popped Screws/Nails Walls	Per	8	\$	4.00	\$ 5	\$	37
	U	Wall - Cracks - Plasterboard - Rake & Stop	Lm	1	\$	12.00	\$ 14	\$	14
Carran tan Daam	V	Walls - Paint - Repaint	Per	3	\$	12.00	\$ 14	\$	42
Computer Room	V	Wall - Cracks - Plasterboard - Rake & Stop	Lm	5 20	\$	12.00	\$ 14 \$ 14	\$	70 280
		Walls - Paint - Repaint Popped Screws/Nails Walls	m2 Per	6	\$	12.00 4.00	\$ 5	\$	28
Middle West Office	W	Wall - Cracks - Plasterboard - Rake & Stop	Lm	0.15	\$	12.00	\$ 14	\$	20
whale west office	VV	Window Frame - Paint -Repaint	m2	6.5	\$	20.50	\$ 24	•	155
North West Office	Х	Wall - Cracks - Plasterboard - Rake & Stop	Lm	10	\$	12.00	\$ 14		140
North West Office	^	Walls - Paint - Repaint	m2	30	\$	12.00		•	420
North 10ffice	Υ	Wall - Cracks - Plasterboard - Rake & Stop	Lm	17	\$	12.00			238
THOREM 10 mee		Walls - Paint - Repaint	m2	41	\$	12.00		•	574
North 2 Office	Z	Wall - Cracks - Plasterboard - Rake & Stop	Lm	5.5	\$	12.00		\$	77
		Walls - Paint - Repaint	m2	30	\$		\$ 14	•	420
		Popped Screws/Nails Walls	Per	2	\$	4.00		\$	9
		Labour - Handyman (Incl. Vehicle)	h	8	\$	32.90	\$ 38	\$	307
Outside Building D	Α	vvali Cracks - General any Substrate - Nake, NTV	Lm	2	\$	10.00	\$ 12	\$	23
North	В	WditCracks's General any substrate - nake, hiv	Lm	12	\$	10.00	\$ 12	\$	140
		Walls - Paint - Repaint	m2	31.5	\$	12.00	\$ 14	\$	441
Office North Outside	С	Wall - Cracks - Exterior Stucco -	Lm	34	\$	17.00		•	674
		Walls - Paint - Repaint	m2	55	\$	12.00		•	770
Entrance Office	D	Grind And fill -Sealant	Lm	1.5	\$	25.00		\$	44
South outside	E	Grind And fill -Sealant Concrete	Lm	1.5	\$	25.00	\$ 29	\$	44
Building E Verhicle	Α	Glazing - Reinstall or replace rubber seals. Up to 1	m2	0.5	\$	120.00	\$ 140	\$	70
Work shop East Wall	В	m2 standerd glass Reseal joins Tilt Panals	Lm	8	\$	25.00	\$ 29	\$	233
Last Wall	Ь	Walls - Paint - Repaint	m2	4	\$	12.00		\$	56
		Mobil Scaffold	Day	1	\$	25.00		\$	29
Workshop 2 SW corner	С	Weld Weld plates to Portal -Epoxy below bottom	Price	1	\$	250.00		•	292
Ceiling	D	plate and reseal Re fit Tiles	Hr	1	\$	40.00	\$ 47	Ś	47
Ceiling	U	Lift - Scissor lift 6m	day	1	\$	100.00			117
			Bothw					•	
Morkshan 2	_	Lift - Scissor lift 6m transport	ays	1	\$	90.00			105
Workshop 3	E	Seal cracks east wall left side Wall Cracks - General any substrate - Rake, RTV	Lm	6.2	\$	25.00	\$ 29	\$	181
Outside Building North	F	and touch up.	Lm	10.6	\$	10.00	\$ 12	\$	124

DAMAGED AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	Rate (\$)	Rate Including CCL fee	Cost included CCL Fee
East Wall	G	Wall Cracks - General any substrate - Rake, RTV and touch up.	Lm	4	\$ 10.00	\$ 12	\$ 47
		Walls - Paint - Repaint	m2	6.2	\$ 12.00	\$ 14	\$ 87
South	Н	Ceiling Cracks - General any substrate - Rake, RTV and touch up.	Lm	3.4	\$ 12.00	\$ 14	\$ 48
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		•	-	• -	EX GST	TOTAL	\$ 43,170

Clarifications / Notes

Ref.

General Rates assume works are carried out in normal works hours without penal labour rates.

General No Allowance for Resource or Buildings Consents as and if they prove to be necessary

General No allowance for removal of furniture and fixtures that may prove necessary (joinery shop)

Work can commence 2 - 4 weeks from receipt of PO.

The project will take approximately 4 weeks to complete.

AREA (ROOM)	Ref No	WORK REQUIRED (DETAILED SCOPE OF WORK)	Unit	Quantity	Rate (\$	5)	Rate Includir fee	ng CCL	
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