# Office and Cafeteria Building – Christchurch Wastewater Treatment Plant – Detailed Engineering Evaluation BU 0879-016 EQ2 Qualitative Report

Prepared for Christchurch City Council

By Beca Carter Hollings & Ferner Ltd (Beca)

2 April 2014



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# **Revision History**

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# **Document Acceptance**

Action	Name	Signed	Date			
Prepared by	Vini Moelianto	pundiper	02/04/2014			
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on behalf of	Beca Carter Hollings & Ferner Ltd					



# Office and Cafeteria – Christchurch Wastewater Treatment Plant BU 0879-016 EQ2

**Detailed Engineering Evaluation Qualitative Report – SUMMARY** Version 2

Address Shuttle Drive Bromley



# **Background**

This is a summary of the Qualitative report for the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

The Office and Cafeteria building is located at Christchurch Wastewater Treatment Plant (CWTP), Shuttle Drive, Bromley. It was originally built in 1979 and has an approximate floor area of 500m<sup>2</sup> internally.

# **Key Damage Observed**

According to the visual inspections on 1 and 14 February 2012, the building has suffered only minor damage. The key damage observed includes:

- Minor damage to ceiling tiles and grids.
- A few vertical cracks in the masonry mortar to the brickwork cladding.
- Minor cracking of gypsum board in meeting room.
- Separation between external concrete ramp and building.
- Cracking to adjacent retaining wall located 1m at north face of the building and this wall supports the building.

# **Critical Structural Weaknesses**

The following potential Critical Structural Weaknesses have been identified:

- Short columns, due to half height brick infill between the concrete columns in the cafeteria.
- Site characteristics, due to widespread liquefaction observed in the surrounding area.

# Indicative Building Strength (from IEP and CSW assessment)

The building has been assessed to have a seismic capacity in the order of 56% NBS using the NZSEE Initial Evaluation Procedure and is therefore classified as Earthquake Risk.



# Recommendations

It is recommended that:

- In accordance with CCC guidance/policy document 'Guidance for Engineers 2' dated 10 May 2012, no restriction are required to the occupancy of the building.
- A verticality and level survey should be carried out to determine the extent of settlement of the building for insurance purposes.
- Optional further investigations of the structural system may be carried out as part of a quantitative analysis of the building if there is concern about the existing %NBS estimate.
- Intrusive investigation is carried out to confirm that the brick veneer has ties to the timber framing.
- Investigate the structural integrity of the adjacent retaining wall (not considered part of this building or DEE).



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# 1 Background

Beca Carter Hollings & Ferner Ltd (Beca) has been engaged by the Christchurch City Council (CCC) to undertake a qualitative Detailed Engineering Evaluation (DEE) of the Office and Cafeteria building located at Christchurch Wastewater Treatment Plant (CWTP), Shuttle Drive, Bromley.

This report is a Qualitative Assessment of the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

A qualitative assessment involves inspections of the building, a desktop review of existing structural and geotechnical information, including existing drawings and calculations, if available and an assessment of the level of seismic capacity against current code using the Initial Evaluation Procedure (IEP).

The purpose of the assessment is to determine the likely building performance and damage patterns, to identify any potential Critical Structural Weaknesses or collapse hazards, and to make an initial assessment of the likely building strength in terms of percentage of new building standard (%NBS).

At the time of this report, no intrusive site investigation, detailed analysis, or modelling of the building structure has been carried out. Partial architectural drawings were made available, and these have been considered in our evaluation of the building. The building description below is based on a review of the drawings and our visual inspections.

The format and content of this report follows a template provided by CCC, which is based on the EAG document.

# 2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

# 2.1 Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 - Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 - Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee carry out a full structural survey before the building is re-occupied.



We understand that CERA will require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building Act). It is understood that CERA is adopting the Detailed Engineering Evaluation Procedure document (draft) issued by the Engineering Advisory Group on 19 July 2011, which sets out a methodology for both qualitative and quantitative assessments. We understand this report will be used in response to CERA Section 51.

The qualitative assessment includes a thorough visual inspection of the building coupled with a desktop review of available documentation such as drawings, specifications and IEP's. The quantitative assessment involves analytical calculation of the building's strength and may require non-destructive or destructive material testing, geotechnical testing and intrusive investigation.

It is anticipated that factors determining the extent of evaluation and strengthening level required will include:

- The importance level and occupancy of the building
- The placard status that was assigned during the state of emergency following the 22 February 2011 earthquake
- The age and structural type of the building
- Consideration of any Critical Structural Weaknesses
- The extent of any earthquake damage

## 2.2 Building Act

Several sections of the Building Act are relevant when considering structural requirements:

#### Section 112 – Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to any alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

#### Section 115 - Change of Use

This section requires that the territorial authority (in this case Christchurch City Council (CCC)) be satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'. Regarding seismic capacity 'as near as reasonably practicable' has previously been interpreted by CCC as achieving a minimum of 67%NBS however where practical achieving 100%NBS is desirable. The New Zealand Society for Earthquake Engineering (NZSEE) recommend a minimum of 67%NBS.

Section 121 – Dangerous Buildings

The definition of dangerous building in the Act was extended by the Canterbury Earthquake (Building Act) Order 2010, and it now defines a building as dangerous if:

- In the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
- In the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
- There is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a 'moderate earthquake' (refer to Section 122 below); or
- There is a risk that that other property could collapse or otherwise cause injury or death; or



 A territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.

Section 122 - Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property. A moderate earthquake is defined by the building regulations as one that would generate ground shaking 33% of the shaking used to design an equivalent new building.

Section 124 - Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 – Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

#### 2.3 Christchurch City Council Policy

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake of the 4th September 2010.

The 2010 amendment includes the following:

- A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
- A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
- A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
- Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

It is understood that any building with a capacity of less than 33%NBS (including consideration of Critical Structural Weaknesses) will need to be strengthened to a target of 67%NBS of new building standard as recommended by the Policy.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply 'as near as is reasonably practicable' with:

- The accessibility requirements of the Building Code.
- The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

#### 2.4 Building Code

The building code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.



On 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

- a. Hazard Factor increased from 0.22 to 0.3 (36% increase in the basic seismic design load)
- b. Serviceability Return Period Factor increased from 0.25 to 0.33 (80% increase in the serviceability design loads when combined with the Hazard Factor increase)

The increase in the above factors has resulted in a reduction in the level of compliance of an existing building relative to a new building despite the capacity of the existing building not changing.

# 3 Earthquake Resistance Standards

For this assessment, the building's Ultimate Limit State earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The new building standard load requirements have been determined in accordance with the current earthquake loading standard (NZS 1170.5:2004 Structural design actions - Earthquake actions - New Zealand).

No consideration has been given at this stage to checking the level of compliance against the increased Serviceability Limit State requirements.

The likely ultimate capacity of this building has been derived in accordance with the New Zealand Society for Earthquake Engineering (NZSEE) guidelines 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. These guidelines provide an Initial Evaluation Procedure that assesses a building's capacity based on a comparison of loading codes from when the building was designed and currently. It is a quick high-level procedure that can be used when undertaking a Qualitative analysis of a building. The guidelines also provide guidance on calculating a modified Ultimate Limit State capacity of the building which is much more accurate and can be used when undertaking a Quantitative analysis.

The New Zealand Society for Earthquake Engineering has proposed a way for classifying earthquake risk for existing buildings in terms of %NBS and this is shown in Figure 3.1 below.

Description	Grade	Risk	%NBS	Existing Building Structural Performance		Improvement of St	ructural Performance
					_→	Legal Requirement	NZSEE Recommendation
Low Risk Building	A or B	Low	Above 67	Acceptable (improvement may be desirable)		The Building Act sets no required level of structural improvement (veloce charge in use)	100%NBS desirable. Improvement should achieve at least 67%NBS
Moderate Risk Building	B or C	Moderate	34 to 66	Acceptable legally. Improvement recommended		This is for each TA to decide. Improvement is not limited to 34%NBS.	Not recommended. Acceptable only in exceptional circumstances
High Risk Building	D or E	High	33 or Iower	Unacceptable (Improvement	Ľ.	Unacceptable	Unacceptable

# Figure 3.1: NZSEE Risk Classifications Extracted from table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table 3.1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. on average 0.2% in any year). It is noted that the current seismic risk in Christchurch results in a 6% risk of exceedance in the next year.



Building Grade	Percentage of New Building Standard (%NBS)	Approx. Risk Relative to a New Building
A+	>100	<1
A	80-100	1-2 times
В	67-80	2-5 times
C	33-67	5-10 times
D	20-33	10-25 times
E	<20	>25 times

#### Table 3.1: %NBS compared to relative risk of failure

# 4 **Building Description**

#### 4.1 General

Summary information about the building is given in the following table.

Item	Details	Comment
Building name	Office and Cafeteria Building – Christchurch Wastewater Treatment Plant	
Street Address	Shuttle Drive Bromley	
Age	Cafeteria was originally designed in 1979 and it is extended in 1987 (architectural drawing) Office were designed in 1987 (Architectural drawing)	
Description	Single storey office and Cafeteria.	
Building Footprint / Floor Area	L-shape with approx. 500m <sup>2</sup> internally	Excluding roof canopies
No. of storeys / basements	1 storey with no basement	
Occupancy / use	Office / Cafeteria	Importance Level 2
Construction	Mix of concrete, steel and timber construction. <b>Cafeteria</b> : concrete frame construction <b>Cafeteria extension area</b> : steel beams and timber stud walls <b>Office</b> : timber construction	Based on limited architectural drawings available and visual inspections.
Gravity load resisting system	<b>Cafeteria</b> : concrete frame <b>Cafeteria extension area</b> : steel frame with probable existing concrete beams at the connection to the existing cafeteria side and steel post on the other side as the	Based on limited architectural drawings available and visual inspections.

#### Table 4.1: Building Summary Information



Item	Details	Comment
	support Office: Timber wall	
Seismic Load resisting system	Cafeteria: Concrete Frame (assumed). No roof or wall bracing was observed or detailed on drawings. Cafeteria extension area: Plywood lined timber wall construction is assumed Office: internal plywood lined timber walls at regular intervals and in both directions. It is assumed that the roof bracing is GIB board.	Based on limited architectural drawings available and visual inspections.
Foundation system	Concrete slab and foundation strips. It is assumed that the timber frame and concrete frame are fixed to the perimeter strip footing to transfer lateral loads to the foundations.	Based on limited architectural drawings available and visual inspections.
Stair system	N.A.	
Other notable features	Perimeter of building is clad by brick veneer Ceiling type in general is ceiling tiles and some part is gypsum board ceiling (in kitchen area)	Intrusive investigation is required to check for veneer ties.
External works	Asphalt pavement, car parking and retaining wall 1m at north part of the building (3m height) – north side	Intrusive investigation may be necessary to confirm the stability of this retaining wall.
Construction information	Architectural drawings dated 1987	Existing Cafeteria structural drawings not provided. Cafeteria extension area and office, Griffiths Moffat and Partners, 1987
Likely design standard	Cafeteria: NZS4203:1976 Cafeteria extension area and office: NZS4203:1984	Inferred from age of the building.
Heritage status	No heritage status	
Other		

# 4.2 Structural 'Hot-spots'

- Separation differential settlement / movement between different types of construction.
- Cracking to concrete columns at half height infill brick veneer locations due to short column effects.



# **5** Site Investigations

## 5.1 **Previous Assessments**

The building had level 2 rapid assessments undertaken following the February 2011 and December 2011 earthquake events (refer to Appendix D).

No significant damage was noted in these level 2 assessments with the exception of the latest level 2, carried out following the 23 December 2011 earthquake events, which recorded minor damage to the ceiling tiles and minor cracks to GIB. In the latest level 2 rapid assessment the building was assessed as having a G1 rating in the placard system.

A series of damage assessments have previously been undertaken including:

- CWTP earthquake damage minor structural repairs report dated the 20 October 2010 after the September 2010 earthquake.
- CWTP: Post-Earthquake Structural Damage Assessment report dated the 1 April 2011 after the February 2011 earthquake.
- CWTP: Claim Report Civil and Structural Repairs issued on 30 November 2011.

In the report CWTP: Post-Earthquake Structural Damage Assessment, dated 1 April 2011, it was noted that the building appears to be in good condition and does not appear have any signs of significant structural damage due to the earthquake events.

### 5.2 Level 4 Damage Inspection

Visual inspections as part of the level 4 damage assessments were undertaken on 1 and 14 February 2012.

# 6 Damage Assessment

#### 6.1 Damage Summary

The table below provides a summary of damaged that we observed on our inspection visit, together with a qualitative indication of likely repairability (E = Easy, M = Moderate, D = Difficult). Refer to Appendix A for photographs of the observed damage and the recommended repair options.

Damage type	Unknown	Minor	Moderate	Major	Comment	Repariability
settlement of foundations		•			Cracks at north face retaining wall of the building. (level survey and intrusive investigation may be required) Cracking to foundation wall (level survey and intrusive investigation are required)	D
tilt of building	✓				None seen. Level survey may be required to confirm.	
liquefaction	$\checkmark$				Widespread liquefaction observed in	

### Table 6.1: Damage Summary



Damage type	Unknown	Minor	Moderate	Major	Comment	Repariability
					surrounding areas.	
settlement of external ground			✓		Cracks in north face of adjacent concrete retaining wall (level survey and intrusive investigation are required).	D
lateral spread / ground cracks	✓				None observed	
frame		✓			Minor cracking to concrete frame less than 1mm width (refer to Appendix A for typical damage)	E
concrete walls					Not Applicable	
cracking to concrete floors		•			Minor cracking of concrete slab at the front of entrance (refer to appendix A for typical damage) Concrete slab inside the building is covered by vinyl	E
bracing	~				No bracing observed during limited inspection	
precast flooring seating					Not Applicable	
stairs					Not Applicable	
cladding /envelope		✓			Widespread vertical cracks observed at masonry mortar joints (refer to Appendix A for typical damage)	E
internal fit out		✓			Minor cracking in GIB board partitions and ceilings	E
building services	✓				No inspection of services	
other		✓			External timber beam supporting roof canopies at cafeteria has minor crack (refer to appendix A for typical damage)	E

## 6.2 Surrounding Buildings

There is a retaining wall located approximately 1m from the northern part of the building. There are widespread vertical cracks at the retaining wall. The failure of this retaining wall can affect to the building stability. Thus, intrusive investigation related to this retaining wall is required.

There are no adjacent buildings that are close enough to have any effect on this building.

## 6.3 Residual Displacements and General Observations

There was no residual displacement observed during our visual inspection, however a differential settlement survey may be required as part of a further investigation or quantitative assessment.



## 6.4 Implication of Damage

The building has suffered minor structural damage which we believe has not significantly diminished the structural capacity.

# 7 Generic Issues

The following generic issues referred to in Appendix A of the EAG guideline document have been identified as applicable to the Office and Cafeteria:

#### Limited-ductile concrete moment resisting frame

 No generic issue has been identified apart from potential structural irregularity or discontinuity in the building.

# 8 Critical Structural Weaknesses

### 8.1 Short Column

Short columns are observed on the perimeter of the cafeteria building since windows above the brick veneer cladding but unlikely to be significant danger. In order to calculate the impact of short column effect, detailed structural drawings of cafeteria showing the reinforcement are required. As we have been unable to obtain this information, an intrusive survey of this building is required to obtain the reinforcement detail of the columns. Short Column effect coefficient of 0.7 is used to assess the %NBS in the IEP for the cafeteria.

### 8.2 Site Characteristics

Widespread liquefaction was observed in surrounding areas of the Office and Cafeteria building. A Site Characteristic coefficient of 0.7 was used to assess the %NBS in the IEP for all parts of the building.

# 9 Geotechnical Consideration

We have obtained previous geotechnical reports for the Christchurch Wastewater Treatment Plant: the Christchurch Wastewater Treatment Plant Upgrade 1998 Geotechnical Report, and the Proposed Bio solids Drying Facility: Geotechnical Interpretive Report from March 2008. Neither of these reports have boreholes in the vicinity of the Office and Cafeteria. However the ground conditions across the site appear to be fairly consistent, with sand and silty sand logged to up to 20m. These reports state that liquefaction was considered likely in a significant earthquake, with damage as a result of liquefaction and the resultant induced settlements. This is consistent with the damage observed following the recent earthquakes. Widespread vertical cracks at retaining wall adjacent to the building are most likely due to settlement or liquefaction of the ground caused by recent Canterbury earthquake events.

# 10 Survey

We recommend that level and verticality surveys are undertaken to confirm settlement of the building and retaining wall not able to be seen during our visual inspections. Settlement of the building may be a significant insurance entitlement.



# **11 Initial Capacity Assessment**

#### 11.1 %NBS Assessment

The building has had its seismic capacity assessed using the Initial Evaluation Procedure based on the information available. The building's capacity is expressed as a percentage of new building standard (%NBS) and is in the order 56%NBS, as shown below in Table 11.1. These capacities are subject to confirmation by a quantitative analysis which is more detailed. The post-damage capacity is considered to be the same as the original capacity.

#### Table 11.1: Indicative Building Capacities

System	Direction	Seismic Performance in <i>%NB</i> S	Notes
Office and Cafeteria (Timber and concrete construction as lateral resisting system)	Both directions	56%	Using NZSEE Initial Evaluation Procedure. Importance level 2

## 11.2 Seismic Parameters

The seismic design parameters based on current design requirements from NZS1170:2004 and the NZBC clause B1 for this building are:

- Site soil class: D NZS 1170.5:2004 Clause 3.1.3, Soft Soil
- Site hazard factor, Z = 0.3, NZBC, Clause B1 Structure, Amendment 11 effective from 19 May 2011
- Return period factor Ru = 1 NZS 1170.5:2004, Table 3.5, Importance level 2 structure with a 50 year design life.
- Near fault factor N(T,D) = 1 NZS 1170.5:2004, Clause 3.1.6, Distance more than 20 km from fault line.

# 11.3 Expected Structural Ductility Factor

The building comprises timber and concrete construction as the lateral load resisting system. In this IEP, it is assumed that the structure is working together with expected structural ductility is 2.

### 11.4 Discussion of results

The Office and Cafeteria building has been calculated to have a seismic capacity of approximately 56% NBS based on qualitative NZSEE IEP assessment which classifies the building as earthquake risk and seismic grade C. Some assumptions have been made such as the beam material and ductility due to limited drawings being available.

# **12 Initial Conclusions**

- The building has been assessed to have a seismic capacity in the order of 56% NBS and is therefore potentially earthquake risk.
- A number of Critical Structural Weaknesses have been identified. These will need to be further investigated to confirm the building capacity. However, it is probable that strengthening work will be required to address these weaknesses.



# **13 Recommendations**

#### 13.1 Occupancy

In accordance with the CCC guidance/policy document 'Guidance for Engineers 2' dated 10 May 2012, no restrictions are recommended to occupancy of the building as a result of our qualitative assessment.

#### 13.2 Further Investigations, Survey or Geotechnical Work

It is recommended that:

- A verticality and level survey should be carried out to determine the extent of settlement of the building for insurance purposes.
- Optional further investigations of the structural system may be carried out as part of a quantitative analysis of the building if there is concern about the existing %NBS estimate.
- Intrusive investigation is carried out to confirm that the brick veneer has ties to the timber framing.
- Investigate the structural integrity of the adjacent retaining wall (not considered part of this building or DEE)

#### 13.3 Suggested Repairs

- Epoxy grout minor cracking to concrete beams, columns and slab
- Re-point cracking mortar between brick veneer cladding
- Replace damaged gypsum lined timber wall
- Seal the separation between concrete and timber
- A suitable repair for large cracks in foundation wall

# **14 Design Features Report**

The suggested repairs are intended to reinstate the existing structural system hence no additional load paths expected as a result of suggested remedial work.

# **15** Limitations

The following limitations apply to this engagement:

- Beca and its employees and agents are not able to give any warranty or guarantee that all defects, damage, conditions or qualities have been identified.
- Inspections are primarily limited to visible structural components. Appropriate locations for invasive inspection, if required, will be based on damage patterns observed in visible elements, and review of the construction drawings and structural system. As such, there will be concealed structural elements that will not be directly inspected.
- The inspections are limited to building structural components only.
- Inspection of building services, pipework, pavement, and fire safety systems is excluded from the scope of this report.
- Inspection of the glazing system, linings, carpets, claddings, finishes, suspended ceilings, partitions, tenant fit-out, or the general water tightness envelope is excluded from the scope of this report.



- The preliminary assessment of the lateral load capacity of the building is limited by the completeness and accuracy of the drawings provided. Assumptions have been made in respect of the geotechnical conditions at the site and any aspects or material properties not clear on the drawings. Where these assumptions are considered material to the outcome further investigations may be recommended. It is noted the assessment has not been exhaustive, our analysis and calculations have focused on representative areas only to determine the level of provision made. At this stage we have not undertaken any checks of the gravity system, wind load capacity, or foundations.
- The information in this report provides a snapshot of building damage at the time the detailed inspection was carried out. Additional inspections required as a result of significant aftershocks are outside the scope of this work.

This report is of defined scope and is for reliance by CCC only, and only for this commission. Beca should be consulted where any question regarding the interpretation or completeness of our inspection or reporting arises.



Appendix A

Photographs



Aerial photograph of site showing the building

# Damage Plan





Typical crack at masonry mortar

General damage description: Damage to mortar in masonry elements.

Recommended repair: damaged mortar should be removed and masonry re-pointed.



Typical crack at concrete frame (less than 0.4mm crack width)

General damage description: Cracks in concrete structures that do not exceed a width of 0.4mm. These cracks are not likely to have any adverse effect on the structural capacity or durability.

Recommended repair: Epoxy injection of cracks over 0.2 mm in width.



# Typical crack at concrete frame (exceed a crack width of 0.4mm but less than 1mm)

General damage description: Cracks in concrete structures that exceed a crack width of 0.4mm, but less than 1.0mm. These cracks require remedial work.

Recommended repair: The cracks should be repaired with an epoxy or grout injection system.



# Typical crack at concrete slab at outside of the building (exceed a crack width of 0.4mm but less than 1mm)

General damage description: Cracks in concrete structures that exceed a crack width of 0.4mm, but less than 1.0mm. These cracks are not considered essential structural damage.

Recommended repair: The cracks should be repaired with cementitious grout or replaced. Insurance entitlement would probably cover removal and replacement.



Typical crack at concrete frame (exceed 1mm crack width)

General damage description: Cracks in concrete structures that exceed a crack width of 1mm and approximately 150mm or more in length.

Recommended repair: Due to the size of the crack observed the steel has potentially yielded. This may provide justification to break out and reinstate the reinforcing detail in this location. Further investigation may be required to confirm extent of cracking, yielding of reinforcing and to develop suitable repair options.



## Separation between concrete slab and wall

General damage description: Separation between concrete slab and wall exceed a crack width of 1mm. This damage requires remedial work to visible affected area.

Recommended repair: The separation should be filled with backing strip and flexible sealant.



## Crack at timber

General damage description: Cracking to timber beam.

Recommended repair: Replace timber.



## Typical damage to gypsum clad timber wall

General damage description: Crack in timber structure including crack at gypsum board and separation at gypsum board joint.

Recommended repair: Replace damaged gypsum board with GIB.



# Separation between timber column (canopy) and concrete column

General damage description: Separation between timber column and concrete column.

Recommended repair: The separation should be repaired with a sealant.



Typical minor cracking at retaining wall

General damage description: Vertical cracking to retaining wall.

Recommended repair: The cracks should be repaired with epoxy or grout injection system. Level survey is also required to confirm possible sign of ground movement and the tilt of the wall.



Separation at retaining wall construction joint

General damage description: Separation at retaining wall with crack widths that exceeds 1mm.

Recommended repair: Further investigation is required to confirm the extent of separation and damage. Level survey is required to confirm ground movement. Cracks in the retaining are to be repaired with an epoxy or grout injection system.

Appendix B
Existing Drawings













Appendix C

CERA DEE Summary Data

Detailed Engineering Evaluation Summary Data			V1.11
Location			
Building Name:	. CCC Office and Cafeteria Unit	No: Street CPEng No:	David Whittaker 123089
Building Address:	Christchurch Wastewater Treatment Plant	Shuttle Drive Company:	Beca
Legal Description:		Company project number: Company phone number:	5323355 03 366 3521
CPS couth	Degrees	Min Sec	17/04/2012
GPS south GPS east		Inspection Date:	1/02/2012 & 4/02/2012
Building Unique Identifier (CCC)	BU 0879-016 EQ2	Revision: Is there a full report with this summary?	0 Ves
Building Unique Identifier (000).	100013-010 EQ2		ycs
Site			
Site slope:	flat	Max retaining height (m):	Contrach report qualitable for parts of site
Soli type Site Class (to NZS1170.5):	: D	Son Profile (if available):	Geotech report available for parts of site
Proximity to waterway (m, if <100m)	·	If Ground improvement on site, describe:	none
Proximity to cliff base (m, if < 100m): Proximity to cliff base (m, if <100m):		Approx site elevation (m):	17.00
Building			
No. of storeys above ground:	1	single storey = 1 Ground floor elevation (Absolute) (m):	17.00
Ground floor split? Storeys below ground		Ground floor elevation above ground (m):	0.25
Foundation type:	strip footings	if Foundation type is other, describe:	
Building height (m): Floor footprint area (approx):	3.50	neight from ground to level of uppermost seismic mass (for IEP only) (m):	3.5
Age of Building (years):	33	Date of design:	1976-1992
Strengthening present?	no	If so, when (year)?	
Use (around floor):	: other (specify)	And what load level (%g)? Brief strengthening description:	
Use (upper floors):	Office and a fata in		
Use notes (if required) Importance level (to NZS1170.5)	IL2		
Gravity Structure Gravity System:	frame system		
Sitting System.			timber rafter (Office), steel rafter and
Roof	concrete flat slab	describe system slab thickness (mm)	concrete (Cafeteria) 100
Beams	cast-insitu concrete	overall depth x width (mm x mm)	unknown
Columns: Walls:	cast-insitu concrete	typical dimensions (mm x mm)	300X300
Lateral load resisting structure		Note: Define along and across in	timber walls (Office and some part of
		detailed report!	cafeteria), limited ductile concrete
Lateral system along: Ductility assumed. u	other (note)	describe system	moment frame (Cafeteria)
Period along	0.40	0.00 estimate or calculation?	estimated
Total deflection (ULS) (mm):	[	estimate or calculation?	
maximum interstorey denection (OLS) (mm).			
			timber walls (Office and some part of
Lateral system across:	: other (note)	describe system	moment frame (Cafeteria)
Ductility assumed, µ	2.00		
Period across: Total deflection (ULS) (mm):	0.40	0.00 estimate or calculation? estimate or calculation?	estimated
maximum interstorey deflection (ULS) (mm):		estimate or calculation?	
Separations:			
north (mm):	,	leave blank if not relevant	
east (mm): south (mm):			
west (mm):			
Non-structural elements			
Stairs:	other (specify)	describe describe (note equity if exists)	no stair
Roof Cladding	: Metal	describe (note cavity in exists) describe	galvanized steel tray roofing
Glazing	other (specify)		half brick with glass window at top at cafeteria
Services(list):			
Available documentation			
Architectura	partial	original designer name/date	Griffiths Moffat&Partners/1987
Mechanica		original designer name/date	
Electrica		original designer name/date	
Geotech report		original designer name/date	
Damage			
Site performance:	some liquefaction occured at surrounding s	te Describe damage:	
(refer DEE Table 4-2)	none observed		
Differential settlement:	none observed	notes (if applicable): notes (if applicable):	
Liquefaction:	none apparent	notes (if applicable):	liquefaction occurred at surrounding site
Differential lateral spread	none apparent	notes (if applicable):	
Ground cracks: Damage to areas	none apparent	notes (if applicable):	damage to retaining wall
Daniego to alea.			
Building:	areen		
Guiterii Flacard Statis			
Along Damage ratio	0%	Describe how damage ratio arrived at:	
Along Damage ratio Describe (summary):		Describe how damage ratio arrived at: Damage $Partia = (\% NBS(before) - \% NBS(after))$	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary):		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Describe (summary):		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage?		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage?		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage?		$Describe how damage ratio arrived at:$ $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe: Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage?		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe: Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage?	0%       0%       0%       1       0       1	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe: Describe: Describe:	cracking to brick veneer cladding
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage?	<ul> <li>0%</li> <li>0%</li> <li>0%</li> <li>0%</li> <li>no</li> <li>no</li> <li>no</li> <li>yes</li> </ul>	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe: Describe: Describe:	cracking to brick veneer cladding
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Describe: Describe: Describe: Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required:		Describe how damage ratio arrived at: Damage_Ratio = $\frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Desc	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations:		Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations: Along Assessed %NBS before:	0%         0%         1         0%         1	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage?: CSWs: Damage?: Pounding: Damage?: Non-structural: Damage?: Non-structural: Damage?: Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations: Along Assessed %NBS before: Assessed %NBS after:	0%           0%           1           0%           1	Describe how damage ratio arrived at:         Damage_Ratio = $\frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe:	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations: Along Assessed %NBS before: Assessed %NBS before:	0%           0%           1           0%           1	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations: Along Assessed %NBS before: Assessed %NBS after: Across Assessed %NBS before: Assessed %NBS after:	0%           0%           0%           1           0           1	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? CSWs: Damage? Pounding: Damage? Non-structural: Damage? Non-structural: Damage? Non-structural: Damage? Non-structural: Damage? Across Assessed %NBS before: Assessed %NBS before: Assessed %NBS after: Across Assessed %NBS before: Assessed %NBS after:	0%           0%	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	
Along Damage ratio Describe (summary): Across Damage ratio Describe (summary): Diaphragms Damage? CSWs: Damage? Pounding: Damage? Pounding: Damage? Non-structural: Damage? Non-structural: Damage? Recommendations Level of repair/strengthening required: Building Consent required: Interim occupancy recommendations: Along Assessed %NBS before: Assessed %NBS after: Across Assessed %NBS before: Assessed %NBS before: Assessed %NBS before: Assessed %NBS after:	0%         0%         0%         0%         1         00%         1	Describe how damage ratio arrived at: $Damage\_Ratio = \frac{(\% NBS(before) - \% NBS(after))}{\% NBS(before)}$ Describe: Descr	Image: Second state sta

Zone, if designed between 1965 and 1992: B	not required for this age of build not required for this age of build	ing	
Period (from above): (%NBS)nom from Fig 3.3:	along 0.4 16.0%		across 0.4 16.0%
Note:1 for specifically design public buildings, to the code of the day: pre-1965 = 1.25; 1965-1976, Zone A =1.33; 196 Note 2: for RC buildings desi Note 3: for buildings designed prior to 1935	65-1976, Zone B = 1.2; all else 1 igned between 1976-1984, use 1 use 0.8, except in Wellington (1.	.0 .2 0)	1.00 1.2 1.0
Final (%NBS)nom:	along 19%		across 19%
2.2 Near Fault Scaling Factor Near Fault scalin	ng factor, from NZS1170.5, cl 3.1	.6:	1.00
Near Fault scaling factor (1/N(T D) Factor A	along 1		across 1
			•
2.3 Hazard Scaling Factor Hazard factor Z	Z for site from AS1170.5, Table 3	.3:	0.30
	Hazard scaling factor, <b>Factor</b>	B: 3.	.333333333
2.4 Return Period Scaling Factor Build	ding Importance level (from abov	e):	2
Return Period Scalir	ing factor from Table 3.1, Factor	<b>C</b> :	1.00
	along		across
2.5 Ductility Scaling Factor Assessed ductility (less than max in Table 3.2) Ductility scaling factor: -1 from 1976 onwards: or -ku, if pre-1976, from Table 3.2	2.00		2.00
	1.00		1.00
Ductiity Scaling Factor, Factor D:	1.00		1.00
2.6 Structural Performance Scaling Factor: Sp:	0.700		0.700
Structural Performance Scaling Factor Factor E:	1.428571429	1.	.428571429
Structural Performance Scaling Factor Factor E:	1.428571429 <b>91%</b>	1.	.428571429 91%
Structural Performance Scaling Factor Factor E:	1.428571429 91%	1.	.428571429 91%
Structural Performance Scaling Factor Factor E:	1.428571429 91%	1.	.428571429 91%
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E         %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)         3.1. Plan Irregularity, factor A:         insignificant         1         3.2. Vertical irregularity, Factor B:	1.428571429 91%	1.	.428571429 91%
Structural Performance Scaling Factor Factor E:	1.428571429 91% Severe	1.	.428571429 91%
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       %NBSb:         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7	1.428571429 91% severe 0 <sep<.005h< td=""><td>Significant .005<sep<.01h< td=""><td>.428571429 91% Insignificant/none Sep&gt;.01H</td></sep<.01h<></td></sep<.005h<>	Significant .005 <sep<.01h< td=""><td>.428571429 91% Insignificant/none Sep&gt;.01H</td></sep<.01h<>	.428571429 91% Insignificant/none Sep>.01H
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       %NBSb:         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right       1.0         Verified       Difference affert D0 (from Table to right       1.0	1.428571429           91%           Severe           0 <sep<.005h< th="">           0.7</sep<.005h<>	Significant .005 <sep<.01h 0.8</sep<.01h 	.428571429 91% Insignificant/none Sep>.01H 1
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)	Severe           0 <sep<.005h< td="">           6 of H         0.7           6 of H         0.4</sep<.005h<>	1. Significant .005 <sep<.01h 0.8 0.7</sep<.01h 	.428571429 91% Insignificant/none Sep>.01H 1 0.8
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       %NBSb:         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right       1.0         Height Difference effect D2, from Table to right       1.0       Alignment of floors not within 20%         Table for Selection of D2       Table for Selection of D2       Table for Selection of D2	Severe	Significant .005 <sep<.01h 0.8 0.7 Significant</sep<.01h 	428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       4         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right 1.0       1.0         Height Difference effect D2, from Table to right 1.0       1.0       Alignment of floors not within 20%         Table for Selection of D2       5.5 Site Characteristics       Significant       0.7	Severe            0 <sep<.005h< td="">            6 of H         0.7           6 of H         0.4           Severe            ration         0<sep<.005h< td=""></sep<.005h<></sep<.005h<>	Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h< td=""><td>428571429 91% Insignificant/none Sep&gt;.01H 1 0.8 Insignificant/none Sep&gt;.01H</td></sep<.01h<></sep<.01h 	428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       1         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right       1.0         Height Difference effect D2, from Table to right       1.0       Alignment of floors not within 20%         Therefore, Factor D:       1       Table for Selection of D2         3.5. Site Characteristics       significant       0.7	Severe           0 <sep<.005h< td="">           6 of H           0.7           6 of H           0.4           Severe           ration           0<sep<.005h< td="">           0.7           6 of H           0.4           Severe           ration           0<sep<.005h< td="">           0.4</sep<.005h<></sep<.005h<></sep<.005h<>	Significant           .005 <sep<.01h< td="">           0.8           0.7           Significant           .005<sep<.01h< td="">           0.5</sep<.01h<></sep<.01h<>	.428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses:       (refer to NZSEE IEP Table 3.4)         3.1. Plan Irregularity, factor A:       insignificant         3.2. Vertical irregularity, factor B:       insignificant         3.3. Short columns, Factor C:       significant         3.4. Pounding potential       Pounding effect D1, from Table to right       1.0         Height Difference effect D2, from Table to right       1.0         Therefore, Factor D:       1         3.5. Site Characteristics       significant       0.7	Severe           91%           91%           6 of H           0.7           6 of H           0.4           0           0           0           0           0           0           0.4           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7           0.7	1. Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1</sep<.01h </sep<.01h 	.428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       %NBSb:         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right 1.0       1.0         Height Difference effect D2, from Table to right 1.0       Alignment of floors not within 20%         Therefore, Factor D:       1         3.5. Site Characteristics       significant       0.7	Severe           91%           91%           6 of H           0.3 Sep<.005H	1. Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1</sep<.01h </sep<.01h 	428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 1
Structural Performance Scaling Factor Factor E:         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       1         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right 1.0       Table for selection of D1         Alignment of floors within 20%       Separ         Alignment of floors not within 20%       Alignment of floors not within 20%         Stite Characteristics       significant       0.7         3.5. Site Characteristics       significant       0.7         3.6. Other factors, Factor F       For ≤ 3 storevs. max value =2.5. otherwise max value =1.5. no minimum	Severe	1. Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1</sep<.01h </sep<.01h 	428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 1 Across 1.3
Structural Performance Scaling Factor Factor E         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E       %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)       1         3.1. Plan Irregularity, factor A:       insignificant       1         3.2. Vertical irregularity, Factor B:       insignificant       1         3.3. Short columns, Factor C:       significant       0.7         3.4. Pounding potential       Pounding effect D1, from Table to right 1.0.       1         Height Difference effect D2, from Table to right 1.0.       1.0       Alignment of floors not within 20%         3.5. Site Characteristics       significant       0.7         3.6. Other factors, Factor F       For ≤ 3 storeys, max value =2.5, otherwise max value =1.5, no minimum Rationale for choice of F factor, if not 1	Severe           91%           91%           6 of H           0.4           0 <sep<.005h< td="">           6 of H           0.4           0<sep<.005h< td="">           6 of H           0.4           0<sep<.005h< td="">           0<rtd>0           0.4           0.7           oreys           0.7           oreys           1.3</rtd></sep<.005h<></sep<.005h<></sep<.005h<>	1. Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1</sep<.01h </sep<.01h 	428571429 91% 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 Across 1.3
Structural Performance Scaling Factor Factor E         Structural Performance Scaling Factor Factor E         Structural Performance Scaling Factor F         For ≤ 3 storeys, max value =2.5, otherwise max value =1.5, no minimum Rationale for choice of F factor, if not 1         Detail Critical Structural Weaknesses:         (refer to DEE Procedure section 6)         List and:	Severe           91%           91%           6 of H           0.7           6 of H           0.4           0           0           severe           ration           0.4           0.7	Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1</sep<.01h </sep<.01h 	428571429 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 Across 1.3 255865
Structural Performance Scaling Factor Factor E         2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E         %NBSb:         Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)         3.1. Plan Irregularity, factor A:       insignificant         3.2. Vertical irregularity, factor B:       insignificant         3.3. Short columns, Factor C:       significant         3.4. Pounding potential       Pounding effect D1, from Table to right 1.0.         Height Difference effect D2, from Table to right 1.0.       Table for selection of D2         3.5. Site Characteristics       significant       0.7         3.6. Other factors, Factor F       For ≤ 3 storeys, max value =2.5, otherwise max value =1.5, no minimum Rationale for choice of F factor, if not 1         Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)       List any:       Refer also section 6.3.1 of DEE for discussion of F f	Severe         91%           91%         0 <sep<.005h< td="">           6 of H         0.7           6 of H         0.4           0<sep<.005h< td="">           ioreys         0.4           ioreys         0.7           ioreys         1           Along         1.3           factor modification for other critic         0.61</sep<.005h<></sep<.005h<>	Significant           .005 <sep<.01h< td="">           0.8           0.7           Significant           .005<sep<.01h< td="">           0.7           0.9           1</sep<.01h<></sep<.01h<>	.428571429 91% 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 Across 1.3 PSSes 0.61
Structural Performance Scaling Factor Factor F         Structural Performance Scaling Factor F         For ≤ 3 storeys, max value =2.5, otherwise max value =1.5, no minimum Rationale for choice of F factor, if not 1         Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)         List any:         Structural Performance Achievement ratio (PAR)	Severe           91%           91%           Severe           ration           0 <sep<.005h< td="">           6 of H           0.4           soreys           0.4           soreys           0.7           oreys           1.3           factor modification for other critic           0.61</sep<.005h<>	Significant .005 <sep<.01h 0.8 0.7 Significant .005<sep<.01h 0.7 0.9 1 1</sep<.01h </sep<.01h 	.428571429 91% 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 Across 1.3 95565 0.61 E69/
Structural Performance Scaling Factor Factor F E         2.7 Baseline %NBS, (NBS%)b = (%NBS)hom x A x B x C x D x E       %NBSb:	Severe         91%           91%         0 <sep<.005h< td="">           6 of H         0.7           6 of H         0.4           oreys         0.4           oreys         0.7           oreys         1.3</sep<.005h<>	Significant           .005 <sep<.01h< td="">           0.8           0.7           Significant           .005<sep<.01h< td="">           0.7           0.9           1</sep<.01h<></sep<.01h<>	428571429 91% 91% Insignificant/none Sep>.01H 1 0.8 Insignificant/none Sep>.01H 1 1 Across 1.3 95585 0.61 56%

Appendix D

Previous Reports and Assessments

OFFICE & CAFETARIA

Reference no.	Room no.	Internal (I)/External (E)	Description of the damage	crack width (MM)	Repair type
0		E	VERTICAL CRACK IN BRICKWORK	0.5	
Û		E	Ц	¢1	
3		E	MORIZONTAL CRACKS IN CONCRETE	0.1/0.2	
4		E	10	10	
5		E	ROTTING, CRACKED TIMBER BEAM		
6)		E	SEPERATION BETWEEN TIMBER		
A)		E	ORAELA IN CONCRETE BEAM	0.3	
(8)		B	ORACK IN CONCRETE FOUNDATION	3. C	
0		e	SEPERATION BETWEEN CONCRETE STEPS & WALL.	10.	
(6)		ŧ	VERTICAL CRACK IN BRITCHWORK	0.2	
0		Ľ	CRACKING TO CONORETE SUAB	0.4	
(12)		F ·	VERTICAL CRACK IN BRICHWORK MURTAR, MISSING CILL TILES		
(13)		E	VERTICAL CRARK IN BRICKWORK MORTAK		
(14)		E	CRACKING TO CONCRETE SLAB (MAY BE EXISTING)		

Reference no.	Room no.	Internal (I)/External (E)	Description of the damage	Crack	width (mm)	Repair type
(21)			ORACKING AT GIB BOARD JUNCTION			
(16)			M			
(7)			((			
			ORACE AROUND COLUMN IN CALING			
(19)			OPACK BETWE IN AUG			
			ORACK IN COULING GIB			
Eb.	_		WATER DAMAGE TO CELLING A WALL			
22/			ORACK IN GIB			
(23)			CEILING GRID MOVED			
(24)			ORACK IN AIB			
(23)			ORACK IN GIB-DOOR OPENING			
(26)			DAMAGE TO CELING GRIP.			

# OFFICE & CAFETARIA





# Aler to inportant note: Structural Inspection attached Christchurch Eq RAPID Assessment Form - LEVEL 2

Inspector initials	PRV	V	Date	23/12/11		Final Pos	ting	INSPECTED	
remtonal Authomy	Christenuren		lime	<del>7</del> :30P		(e	.g. UNSAFE)	<u> </u>	
Building Name	ADMINUS	- A 4							$\mathbf{i}$
	AUTINIS	TLATION (JI	<u>MLQING.</u> Tyl	be of Constructi	ion				
1001033	CWIP	<u> </u>	K	Timber frame	•		Concrete she	ar wali	
GPS Co-ordinates	S0	<b>—</b>	Ľ	Steel frame			Unreinforced	masonry	
Contact Name	0040.00	<u> </u>		I III-Up concre	te		Reinforced ma	asonry	
Contact Phone	027435 6	<u>CK Gezz</u>	AGGAL)	RC frame with	ne n masonry Infil		Confined mase Other:	onry	
Storeys at and above ground level	1	Below ground level	Prin	nary Occupancy Dwelling	y	X	Commercial/ C	ffices	
Total gross floor area (m²)		Year built -	_ 0	Other resident	ia!		Industrial		
No of residential Units	Ø			Public assemb	bly		Government		
	~			School			Heritage Listed		
Photo Taken	Yes)	No		Religious			Other		
Investigate the building for	the conditions list	ed on page 1	and 2, and ch	eck the approp	priate columi	n. A sketch	n may be added	on page 3	
Overali Hazards / Damage	e Mino	or/None a	Aoderate	Severe			Comments	on page o	
Collapse, partial collapse, off fi	oundation	X			No si	anitica	of star	buril dan	Wird
Building or storey leaning		X			abert	dan	dan	anna rent	T
Wall or other structural damage	)				reducto	N in	startur	al canad	<u>h.</u>
Overhead falling hazard	I	X			tam 2	2/12/2	i EO	<u>u cupuch</u>	<u>y</u> _
Ground movement, settlement,	slips				Jun c	SALCA	1.2.0.		
Neighbouring building hazard	I	X				<u> </u>			
Electrical, gas, sewerage, water	, hazmats	X							
Record any exis	ting placard on	this building	j:	Existi Placa	ing rd Type				<u> </u>
Choose a new posting grounds for an UNSA INSPECTED placard a of this page	y based on the new FE posting. Local t main entrance. P	w evaluation a ised Severe a lost all other (	and team judg Ind overall Mon placards at eve	(e.g. L ement. Severe derate condition ery significant e	JNSAFE) conditions at ns may requi entrance. Tra	ffecting the ire a RESTR Insfer the c	whole building RICTED USE. Pl hosen posting t	are ace the top	
INSPECTI	ED 🔨	F	RESTRICTED	IISF					
GREI		2	YEL	LOW Y1	Y2	RED	R1 R2	R3	
Further Action Recor	nmended:	y.							
Tick the boxes below (	only if further action deri (state location	s are recommi	ended						
Detailed engineering	g evaluation recon	/· Imended							
Structur	al	Geotecl	hnical	C Other:	:				/
Other recommenda	fions:								/
Estimated Overall Building D	amage (Exclude	Contents)		-	·····	Sign he	ere on completion		
None	64 00	_				This	the		
0-1% ⊡ 2-10% ⊠	31-60 % 61-00 %						as had		
11-30 %	100 %				Date & Tin ID	ne .	<u>zs/k/i</u>		

Inspection ID: \_\_\_\_\_ (Office Use Only)

Structural Hazards/ Damage Foundations Roofs, floors (vertical load)	Minor/None Ki	Moderate	Severe	Comments
Columns, pilasters, corbels	$\mathbf{X}$			
Diaphragms, horizontal bracing	$\mathbf{X}$			
Pre-cast connections				
Beam				
Non-structural Hazards / Damage				
Parapets, omamentation	$\mathbf{X}$			Minor damage Lada II
Cladding, glazing	×			and fill the certific fler
Ceilings, light fixtures		$\mathbf{X}$	n	Curu light openices
Interior walls, partitions				superficial crucks to internal
Elevators	X		<u>п</u> .	<u> </u>
Stairs/ Exits	X			
Utilities (eg. gas, electricity, water)	X			
Other		Π		
Geotechnical Hazards / Damage			- Lai	·····
Siope failure, debris	X			
Ground movement, fissures	X			
Soil bulging, liquefaction	X			
General Comment <u>Overall</u>	<u>no sìgnì</u>	kcont	structur	al damage observed.

# Usability Category

Damage Intensity	/ Posting	Usability Category	Remarks
Light damage	Inspected	G1. Occupiable, no immediate further investigation required	Morren finites de cost on tit
Low risk	(Grøen)	G2. Occupiable, repairs required	and repair Areplace where
Medium damage	Restricted Use (Yellow)	Y1. Short term entry	
Vedium risk		Y2. No entry to parts until repaired or demolished	
eavy damage		R1. Significant damage: repairs, strengthening possible	
igh risk	Unsafe (Red)	R2. Severe damage: demolition likely	
		R3. At risk from adjacent premises or from ground failure	

Sketch (optional) Provide a sketch of the entire					T	T						T	7			
damage points. Indicate damage points.	-														+	
		+-	+		+-			_						$\square$		
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				:						+-						
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			_							+	+					

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# Recommendations for Repair and Reconstruction or Demolition (Optional)

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\_\_\_\_

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8. M

3 Inspection ID: \_\_\_\_\_ (Office Use Only)

# Important Note: Structural Inspection

#### 1.1 Background

Beca has carried out an inspection of the following building following the Dec 23<sup>rd</sup> earth

Building Name	Administration	Rubling	eannquakes
Building Address	CWTP	uning	
Date:	23/12/11		

#### **Basis of inspection** 1.2

This Level 2 rapid assessment has been prepared based upon limited visual inspection, and is intended to record the damage caused by the aftershocks of 23 December 2011. In all other respects, it is not intended to supersede previous more detailed inspections and reports. It's scope is confined to assessing the likely effect of observed damage upon the building lateral capacity, to establish the degree to which this has been diminished (relative to the building in its undamaged state). It does not serve as a substitute for an IEP (or more detailed seismic assessment) which provides an assessment of the building against current code requirements and hence quantifies the risk presented by the building relative a building designed in accordance with modern codes.

#### Earthquake Prone Buildings 1.3

We will attempt to review work Beca has completed on the above building including highlighting again if this is an earthquake prone building. If Beca has no history with the property the onus in on the Manager or Owner to highlight any inspection history and make known who and when

# No State of Emergency, therefore no placard system operational 1.4

No state of emergency has been declared and as such, the emergency placard system has not been activated. Beca will not apply placards as part of this inspection.

#### No observed reduced capacity 1.5

If our inspection indicates no apparent reduced capacity this does not mean that the building is declared safe to occupy by Beca. This means that the building appears to be in no worse state than before 23 December 2011. The ultimate decision on whether to occupy the building

#### 1.6 **Diminished Capacity**

If our inspection indicates diminished capacity, then our recommendation will be to carry out a full IEP assessment. This will need to be prioritised and scheduled once the initial response is over.

#### Badly damaged buildings 1.7

If we have any concern in relation to the level of damage, we will of course highlight this to you. Beca will refer your building for further inspection to the Christchurch Cit Council who have the authority to declare a building unsafe under the Building Act or to CERA who may require further detailed work or demolition under the Canterbury Earthquake Recovery Act 2011.

#### 1.8 **Further Clarification**

If you require further clarification on the important points above, please contact one of the following:

Jonathan Barnett; Acting Section Manager Beca Christchurch Structural: 027 207 0860

Mark Spencer; General Manager Beca Structural Engineering; 021 370 ア 56

Craig Price; South Island Regional Manager; 027 488 4123

#### Scope of Services 2

a. Our building inspections will be initially limited to structural inspections in accordance with the Level 2 Rapid Structural Safety Assessments guidelines identified above. While these guidelines assume that the inspections will be carried out for a territorial authority during a state of emergency, our work will be carried out for you (instead of for a territorial authority), and will continue to be carried out, in line with the guideline, after the state of emergency has been lifted. Our inspections will be for the sole purpose of providing an urgent assessment of the damage to key structural elements of a building that may pose a risk for life safety and access purposes, and are based on an internal and an external visual inspection of key elements of the structure readily accessible at the time of the inspection. The assessment may include recommendations for work to be done under urgency where there is a need to demolish or secure the structure to ensure the safety of the public or protect adjacent property.

We will be passing the Level 2 Assessment forms to the Christchurch City Council and/or CERA. We believe from discussions with the Council that these reports will fulfil their requirements for Level 2 assessments for these buildings and the Council will not separately

- b. Beca and its employees and agents are not able to give any warranty or guarantee that all defects, damage, conditions or qualities have been identified and further post disaster engineering advice should be sought regarding a detailed inspection of the building and the detailed repair and remedial work required on the building to restore functionality and Building Code compliance. Beca liability for any loss, damage, costs, or claim arising due to, or in connection with the assessment for any particular building and any related advice is limited to direct property damage and shall not exceed the fees rendered by Beca for that particular
- c. The inspections will not cover building services systems however such inspections and any advice on detailed repair or remedial work for these systems can be undertaken in association with other post disaster engineering advice at your request.
- d. The terms of this letter and the conditions of engagement described below will continue to apply to all services performed by Beca in respect of the buildings for which this commission applies unless and until new written conditions of engagement are entered into.

# 3 Conditions of Engagement

The conditions that will apply to our Services are the ACENZ/IPENZ Short Form Model Conditions of Engagement (Commercial), dated April 2007 (the "Conditions"), a cop y of which is attached, with the following two modifications:

- Point 2.b. above under our scope of services prevails over the Conditions, including the amount of our liability; and
- Although we will apply the standard of care in accordance with clause 2 of the Conditions, such standard will be applied in the context of the scope of services above, including the urgency we will need to work, the limited nature of the inspections, and the limited information available to us.

# 4 Acknowledgement

I confirm I have read the above and will liaise with and advise the building owner/tenants accordingly.

	Building Owner/Manager	Name: CC.C GRAENE BLACK Signature:
	Beca Engineer	Name: PHIL WILKINS Signature: Manths
ſ	Date	23/12/11

#### **Beca Staff Present:**

Name	Signature	
GRAGHE WELLS		

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C C	hristch	urch Ed		D /	Issos	Emor	AP	-	i.	JTPI	
- IOSpector Initials	1.1	/			CELER	smer	it For	- m	LEVE	L 2	
Territorial Authority	Chris	tchurch City	Da	le no	711	//	Fina	Posti	ng		
Building Name	Christer	web luce	Louita .		1010	·		(e.g	UNSAFE)	Grl	
Short Name	· Admin	istration R.	vildian	Tv	H <b>nc</b> nl De of Eone	Plant					
Address	shufle	DINE		 [1]	Timherd	oucuon forma		~	/		
	Bomles	, Christian	ych	-0	Steel fra			N	Concrete she	ar wali	
GPS Co-ordinates	<u>5°</u>	Eº			Till-up o	000rete		Ц	Unreinforced	masonry	
Contact Name	Mike	Bourke			Concrete	frame			Reinforced ma	sonry	
Contact Phone	02)2	130698			RC fram	e with mason	rv infil		Confined mass	onry	
Storeys at and above		Below		Prim	ary Occup	anev	iy nina		Other;		
ground level	_1	level	0		Dwelling	-,					
(m²)	× 400	Year		~	0				Commercial/ O	ffices	
No of residential ( Inits					Uther res	idential		<b>1</b>	ndustrial		
I Cinta		<u> </u>			Public ass	sembly			Sovernment		
Photo Taken	Yes	(No)			School			Пн	leritage Listed		1
Investigate the building fi	or the condition	ns listed on mar			Religious		_		Other		
Overall Hazards / Dama	ge	Minor/None	ye 1 and 2, a Moderne	រោថ chi	eck the ap	propriate co	olumn, A s	ketch m	ay be added	P 4060 10	
Coltapse, partial collapse, d	f foundation			-	Severe			¢	omments		
Building or storey leaning									·····		
Wall or other structural dama	ige										
Overhead falling hazard		Ē.									
Ground movement, settlemer	nt, slips										
Neighbouring building hazard											
Electrical, gas, sewerage, wa	ter, hazmars		- -			· <u> </u>					
Record any ex	isting placar	d on this build	ling:		Ev	intia a					
k			-		Pla	acard Type				]	
Choose a new posti	NO based on H	IG BRIN and Lot			<b>(</b> B.	g. UNSAFE					- )
grounds for an UNS	AFE posting.	Localised Sever	on and team j re and overal	judger I Mode	Nent. Sev	ere conditio	ns affectin	g the w	hole building		
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INSPECT	TED			-		-		-	- Posting D	the top	
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Record any restrict	ion pruse or	entry:	i			1 1 12	R	ED	R1 R2	R3	
Further Action Reco	un manala J.									·	
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csumated Overall Building	Damage (Exc	ude Contents)									
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2-10% LM	31-6	0% [ 0% -	2			-	NHA	Un/ V	(Beca	)	
11-30 %	100 1	5% [ % r				Date &	Time	5	13/11		
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Structural Hazards/ Damage	Minor/Norie	Moderate	Severe	cwsp]	Comments	د. د. ب
Roofs, floors (vertical load)			П			
Columns, pilasters, corbels				<u> </u>		
Diaphragms, horizontal bracing						
Pre-cast connections						
Beam	M					
Non-structural Hazards / Damage	/					
Parapets, ornamentation	Z,					
Cladding, glazing					<u></u>	
Ceilings, light fixtures						
Interior walls, partitions	e					
Elevators IV/					<u></u>	
Stairs/ Exits						
Utilities (eg. gas, electricity, water)	Ľ			•		
Other						
Geotechnical Hazards / Damage						
Slope failure, debris	Ø					
Ground movement, fissures						
Soil bulging, liquefaction				· Evidence o	1 lignataction	erevel.
General Comment The build	ilding appe	cars to	be in a	side word His.	with no and	erch
structural	<i>I</i>					
					··	
	-					

Usability Category

Damage Intensity	Posting	Usability Category	Remarks
Light damage	(Green)	G1. Occupiable, no immediate further	
Low risk		G2. Occupiable, repairs required	
Medium damage	Restricted Use (Yellow)	Y1. Short term entry	
Medium risk		Y2. No entry to parts until repaired or demolished	
	Unsafe (Reď)	R1. Significant damage: repairs, strengthening possible	\
rieavy oanlage Hinh risk		R2. Severe damage: demolition likely	
rnyn nas		R3. At risk from adjacent premises or from ground failure	

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2 Inspection ID: \_\_\_\_\_ (Office Use Only)

Sketch (optional) Provide a sketch of the entire		CWTPI
building or damage points, Ind damage points,	cafe	
6		
•		
Recommendations for Repair a	nd Reconstruction or Demotiving (0, in a	
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- <b>-</b>		
5		
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