



Christchurch City Council

**Victoria Park
Resource Building
PRK 1829 BLDG 013**

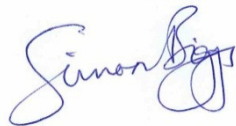
**Detailed Engineering Evaluation
Qualitative Assessment Report**



Christchurch City Council

Victoria Park Resource Building Qualitative Assessment Report

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Summary

Victoria Park Resource Building
PRK 1829 BLDG 013

Detailed Engineering Evaluation
Qualitative Report - Summary
Final

Background

This is a summary of the qualitative report for the Victoria Park Resource Building, and is based on the Detailed Engineering Evaluation Procedure document (draft) issued by the Structural Advisory Group on 19 July 2011.

Key Damage Observed

The resource building suffered minor damage of non-structural elements. This consisted predominantly of ceiling battens missing on one side of the building.

Critical Structural Weaknesses

No critical structural weaknesses were found in the building

Indicative Building Strength

The resource building has an estimated seismic capacity of 83% NBS and is therefore classified as a low risk building in accordance with NZSEE guidelines.

Recommendations

The building has achieved a capacity of 83% NBS, therefore there is no requirement to strengthen the lateral load resisting elements.

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1 Introduction

Opus International Consultants Limited has been engaged by Christchurch City Council to undertake a detailed seismic assessment of Victoria Park Resource Building, located at 101 Victoria Park Road, Cashmere, Christchurch following the Canterbury Earthquake Sequence since September 2010.

The purpose of the assessment is to determine if the building is classed as being earthquake prone in accordance with the Building Act 2004.

The seismic assessment and reporting have been undertaken based on the qualitative and quantitative procedures detailed in the Detailed Engineering Evaluation Procedure (DEEP) document (draft) issued by the Structural Engineering Society (SESOC) [3] [4].

2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

2.1 Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 – Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 – Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee to carry out a full structural survey before the building is re-occupied.

We understand that CERA require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building Act). CERA have adopted the Detailed Engineering Evaluation Procedure (DEEP) document (draft) issued by the Structural Engineering Society (SESOC) on 19 July 2011. This document sets out a methodology for both initial qualitative and detailed quantitative assessments.

It is anticipated that a number of factors, including the following, will determine the extent of evaluation and strengthening level required:

1. The importance level and occupancy of the building.

2. The placard status and amount of damage.
3. The age and structural type of the building.
4. Consideration of any critical structural weaknesses.

Christchurch City Council requires any building with a capacity of less than 34% of New Building Standard (including consideration of critical structural weaknesses) to be strengthened to a target of 67% as required under the CCC Earthquake Prone Building Policy.

2.2 Building Act

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 - Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to the alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

The Earthquake Prone Building policy for the territorial authority shall apply as outlined in Section 2.3 of this report.

Section 115 – Change of Use

This section requires that the territorial authority is satisfied that the building with a new use complies with the relevant sections of the Building Code ‘as near as is reasonably practicable’.

This is typically interpreted by territorial authorities as being 67% of the strength of an equivalent new building or as near as practicable. This is also the minimum level recommended by the New Zealand Society for Earthquake Engineering (NZSEE).

Section 121 – Dangerous Buildings

This section was extended by the Canterbury Earthquake (Building Act) Order 2010, and defines a building as dangerous if:

1. In the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
2. In the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
3. There is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a ‘moderate earthquake’ (refer to Section 122 below); or
4. There is a risk that other property could collapse or otherwise cause injury or death; or

5. A territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.

Section 122 – Earthquake Prone Buildings

This section defines a building as earthquake prone (EPB) if its ultimate capacity would be exceeded in a ‘moderate earthquake’ and it would be likely to collapse causing injury or death, or damage to other property.

A moderate earthquake is defined by the building regulations as one that would generate loads 33% of those used to design an equivalent new building.

Section 124 – Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 – Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

2.3 Christchurch City Council Policy

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake on 4 September 2010.

The 2010 amendment includes the following:

1. A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
2. A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
3. A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
4. Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply ‘as near as is reasonably practicable’ with:

- The accessibility requirements of the Building Code.

- The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

Where an application for a change of use of a building is made to Council, the building will be required to be strengthened to 67% of New Building Standard or as near as is reasonably practicable.

2.4 Building Code

The Building Code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.

On 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

- increase in the basic seismic design load for the Canterbury earthquake region (Z factor increased to 0.3 equating to an increase of 36 – 47% depending on location within the region);
- Increased serviceability requirements.

2.5 Institution of Professional Engineers New Zealand (IPENZ) Code of Ethics

One of the core ethical values of professional engineers in New Zealand is the protection of life and safeguarding of people. The IPENZ Code of Ethics requires that:

Members shall recognise the need to protect life and to safeguard people, and in their engineering activities shall act to address this need.

- 1.1 *Giving Priority to the safety and well-being of the community and having regard to this principle in assessing obligations to clients, employers and colleagues.*
- 1.2 *Ensuring that responsible steps are taken to minimise the risk of loss of life, injury or suffering which may result from your engineering activities, either directly or indirectly.*

All recommendations on building occupancy and access must be made with these fundamental obligations in mind.

3 Earthquake Resistance Standards

For this assessment, the building's earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed

as a percentage of new building standard (%NBS). The loadings are in accordance with the current earthquake loading standard NZS1170.5 [1].

A generally accepted classification of earthquake risk for existing buildings in terms of %NBS that has been proposed by the NZSEE 2006 [2] is presented in Figure 1 below.

| Description | Grade | Risk | %NBS | Existing Building Structural Performance | Improvement of Structural Performance | |
|------------------------|--------|----------|-------------|---|---|---|
| | | | | | Legal Requirement | NZSEE Recommendation |
| Low Risk Building | A or B | Low | Above 67 | Acceptable (improvement may be desirable) | The Building Act sets no required level of structural improvement (unless change in use) This is for each TA to decide. Improvement is not limited to 34%NBS. | 100%NBS desirable. Improvement should achieve at least 67%NBS |
| Moderate Risk Building | B or C | Moderate | 34 to 66 | Acceptable legally. Improvement recommended | | Not recommended. Acceptable only in exceptional circumstances |
| High Risk Building | D or E | High | 33 or lower | Unacceptable (Improvement required under Act) | Unacceptable | Unacceptable |

Figure 1: NZSEE Risk Classifications Extracted from table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table 1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. 0.2% in the next year).

Table 1: %NBS compared to relative risk of failure

| Percentage of New Building Standard (%NBS) | Relative Risk (Approximate) |
|--|-----------------------------|
| >100 | <1 time |
| 80-100 | 1-2 times |
| 67-80 | 2-5 times |
| 33-67 | 5-10 times |
| 20-33 | 10-25 times |
| <20 | >25 times |

3.1 Minimum and Recommended Standards

Based on governing policy and recent observations, Opus makes the following general recommendations:

3.1.1 Occupancy

The Canterbury Earthquake Order¹ in Council 16 September 2010, modified the meaning of “dangerous building” to include buildings that were identified as being EPB’s. As a result of this, we would expect such a building would be issued with a Section 124 notice, by the Territorial Authority, or CERA acting on their behalf, once they are made aware of our assessment. Based on information received from CERA to date and from the DBH guidance document dated 12 June 2012 [6], this notice is likely to prohibit occupancy of the building (or parts thereof), until its seismic capacity is improved to the point that it is no longer considered an EPB.

3.1.2 Cordoning

Where there is an overhead falling hazard, or potential collapse hazard of the building, the areas of concern should be cordoned off in accordance with current CERA/territorial authority guidelines.

3.1.3 Strengthening

Industry guidelines (NZSEE 2006 [2]) strongly recommend that every effort be made to achieve improvement to at least 67%NBS. A strengthening solution to anything less than 67%NBS would not provide an adequate reduction to the level of risk.

It should be noted that full compliance with the current building code requires building strength of 100%NBS.

3.1.4 Our Ethical Obligation

In accordance with the IPENZ code of ethics, we have a duty of care to the public. This obligation requires us to identify and inform CERA of potentially dangerous buildings; this would include earthquake prone buildings.

¹ This Order only applies to buildings within the Christchurch City, Selwyn District and Waimakariri District Councils authority

4 Building Description

4.1 General

The Victoria Park Resource Building is a single storey timber framed structure with timber planks wall cladding and a corrugated iron roof. The timber framed floor is supported on concrete piles.

The building is approximately 10m long in the east-west direction and 7m wide in the north-south direction. The apex of the roof is approximately 2.7m from the ground and the wall height is approximately 2.35m. An attached verandah is on the northern side of the building. The ceiling is plasterboard or fibrous plaster lined at 2.4m height.

The building age is unknown, but it is expected to have been built before the 1960s.

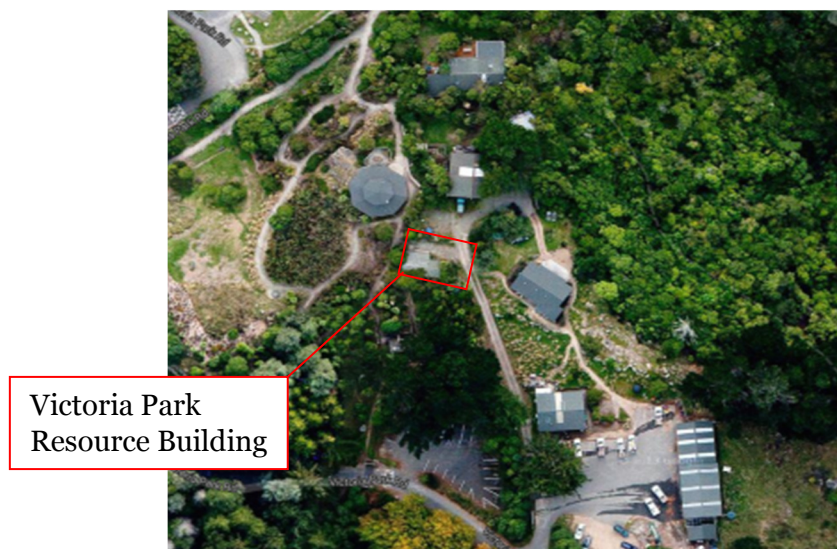


Figure 2: Site plan of Victoria Park indicating location of Resource Building (Source: Google Maps).

4.2 Gravity Load Resisting System

Roof gravity loads are transferred by the timber framed walls supported by a timber floor on concrete piles.

4.3 Seismic Load Resisting System

Lateral loads are resisted by the in-plane bracing capacity of the timber wall framing in both directions. The timber wall framing is assumed to achieve its bracing capacity with nailed sheet lining.

5 Damage Assessment

There was no observed damage although access to the inside was not available at the time. Views through the windows did not reveal any interior damage, other than a missing architrave moulding.

6 Detailed Seismic Assessment

The detailed seismic assessment has been based on the NZSEE 2006 [2] guidelines for the “Assessment and Improvement of the Structural Performance of Buildings in Earthquakes” together with the “Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury, Part 2 Evaluation Procedure” [3] draft document prepared by the Engineering Advisory Group on 19 July 2011, and the SESOC guidelines “Practice Note – Design of Conventional Structural Systems Following Canterbury Earthquakes” [5] issued on 21 December 2011.

6.1 Critical Structural Weaknesses

The term Critical Structural Weakness (CSW) refers to a component of a building that could contribute to increased levels of damage or cause premature collapse of a building.

No CSW's have been identified for this building.

6.2 Seismic Coefficient Parameters

The relevant seismic parameters deemed suitable for this structure for determining the seismic coefficient in accordance with NZS1170.5 are:

- Importance Level 2
- First Period of vibration, $T_1 < 0.4\text{sec}$
- Seismic Hazard Factor, $Z = 0.3$
- Site Subsoil Class C
- Return Period Factor, $R_u = 1.0$
- Near Fault Factor, $N(T,D) = 1.0$
- Structural Ductility Factor, $\mu = 2.5$ (nailed sheet bracing walls)
- Structural Performance Factor, $S_p = 0.7$

6.3 Detailed Seismic Assessment Results

The structure was found to have an estimated seismic capacity of 83% NBS. This is above the threshold limit for structures classified as “Earthquake Prone” which is one third (33%) of the seismic performance specified in the current loading standard for new structures. The building is therefore not considered to be Earthquake Prone in accordance with the Building Act 2004.

6.4 Limitations and Assumptions in Results

The observed level of damage suffered by the building was deemed low enough to not affect the capacity. Therefore the analysis and assessment of the building was based on it being in an undamaged state. There may have been damage to the building that was unable to be observed that could cause the capacity of the building to be reduced; therefore the current capacity of the building may be lower than that stated.

The results have been reported as a %NBS and the stated value is that obtained from our analysis and assessment. Despite the use of best national and international practice in this analysis and assessment, this value contains uncertainty due to the many assumptions and simplifications which are made during the assessment. These include:

- a. Simplifications made in the analysis, including boundary conditions such as foundation fixity.
- b. Assessments of material strengths based on limited drawings, specifications and site inspections
- c. The normal variation in material properties which change from batch to batch.
- d. Approximations made in the assessment of the capacity of each element, especially when considering the post-yield behaviour.

7 Conclusions

The building has an estimated seismic capacity of 83% NBS and is therefore not considered to be Earthquake Prone in accordance with the Building Act 2004.

We do not consider that there is a high risk of collapse or high risk imposed to building occupants. The building has performed well under the recent earthquake events and no critical structural weaknesses or life safety hazards were identified, hence we believe that the building can continue to be fully occupied.

8 Recommendations

The building has achieved a capacity of 83% NBS, therefore there is no requirement to strengthen the lateral load resisting elements.

9 Limitations



- (a) This report is based on an inspection of the structure with a focus on the damage sustained from the 22 February 2011 Canterbury Earthquake and aftershocks only. Some non-structural damage is mentioned but this is not intended to be a comprehensive list of non-structural items.
- (b) Our professional services are performed using a degree of care and skill normally exercised, under similar circumstances, by reputable consultants practicing in this field at the time.
- (c) This report is prepared for the CCC to assist with assessing remedial works required for council buildings and facilities. It is not intended for any other party or purpose.

10 References



- [1] NZS 1170.5: 2004, Structural design actions, Part 5 Earthquake actions, Standards New Zealand.
- [2] NZSEE (2006), Assessment and improvement of the structural performance of buildings in earthquakes, New Zealand Society for Earthquake Engineering.
- [3] Engineering Advisory Group, Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury, Part 2 Evaluation Procedure, Draft Prepared by the Engineering Advisory Group, Revision 5, 19 July 2011.
- [4] Engineering Advisory Group, *Guidance on Detailed Engineering Evaluation of Non-residential buildings, Part 3 Technical Guidance*, Draft Prepared by the Engineering Advisory Group, 13 December 2011.
- [5] SESOC (2011), Practice Note – Design of Conventional Structural Systems Following Canterbury Earthquakes, Structural Engineering Society of New Zealand, 21 December 2011.
- [6] DBH (2012), Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch, Department of Building and Housing, June 2012.

Appendix 1 - Photographs

Victoria Park Resource Building – Detailed Engineering Evaluation

| Victoria Park Resource Building | | |
|---------------------------------|-----------------------------------|--|
| No. | Item description | Photo |
| 1. | Front view of the building |  A photograph showing the front view of a single-story building with dark brown vertical wood siding and a corrugated metal roof. A white-framed window with vertical blinds is visible on the left. A red fire hose reel is mounted on the wall to the right of the window. The building is surrounded by greenery, including tall grasses and trees in the background. A green tarp is visible on the right side of the building. |
| 2. | Veranda roof attached to building |  A close-up photograph of the veranda roof structure. The roof is made of corrugated metal and is supported by dark wooden beams. The building's exterior wall, made of dark brown vertical wood siding, is visible on the left. A window with a white frame is partially visible below the veranda. The background shows green trees. |

Victoria Park Resource Building – Detailed Engineering Evaluation

| | | |
|-----------|--|--|
| <p>3.</p> | <p>Cracked verandah post</p> |  |
| <p>4.</p> | <p>Inside view of wall and ceiling. Side architrave is missing</p> |  |

| | | |
|----|--------------|---|
| 5. | Window frame |  A photograph showing a close-up view of a window frame. The frame is white and appears to be made of wood or a composite material. There is significant wear and tear, including peeling paint and discoloration, particularly around the edges and in the recessed areas. The window glass is visible, reflecting the surrounding environment, which includes trees and a dark roofline. The overall appearance suggests the window is in poor condition and may require repair or replacement. |
|----|--------------|---|

Appendix 2 – CERA DEE Spreadsheet



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