Ascot Community Centre Detailed Engineering Evaluation BU 1306-003 EQ2 Qualitative Report

Prepared for Christchurch City Council (CCC)

By Beca Carter Hollings & Ferner Ltd (Beca)

14 June 2013

© Beca 2013 (unless Beca has expressly agreed otherwise with the Client in writing).

This report has been prepared by Beca on the specific instructions of our Client. It is solely for our Client's use for the purpose for which it is intended in accordance with the agreed scope of work. Any use or reliance by any person contrary to the above, to which Beca has not given its prior written consent, is at that person's own risk.



Revision History

Revision Nº	Prepared By	Description	Date
Α	Andrew Sporn	Draft for CCC review	9 October 2012
В	Andrew Sporn	Final	14 June 2013

Document Acceptance

Action	Name	Signed	Date
Prepared by	Andrew Sporn	affern	14 June 2013
Reviewed by	Nicholas Charman	MKoppe	14 June 2013
Approved by	David Whittaker	Dwitth	14 June 2013
on behalf of	Beca Carter Hollings & Fe	erner Ltd	



Ascot Community Centre BU1306-003 EQ2

Detailed Engineering Evaluation Qualitative Report – SUMMARY Version 1

Address

12 Ascot Avenue, Parklands, Christchurch



Background

This is a summary of the Qualitative report for the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

The Ascot Community Centre is located at 12 Ascot Avenue, Parklands, Christchurch. It is assumed to have been built in 1968 (from information contained in a newspaper article about the opening) and has an approximate floor area of 290m² internally. It is currently used as a multipurpose community hall. The building is generally rectangular in plan and the main structural system comprises of concrete masonry block walls and timber/steel roof framing. No structural drawings were obtained and no calculations were carried out.

Key Damage Observed

Visual inspections on 7 August 2012 indicate the building has suffered minor structural earthquake damage. The key damage observed includes:

- n Cracking in the plasterboard ceiling panels.
- n Minor cracking to the external concrete ground slab under the balustrade outside of the building.
- we understand that there was damage to the internal masonry block walls. This damage appears to have been repaired.

Critical Structural Weaknesses (CSW)

The following Critical Structural Weakness (CSW) was identified based on the structural inspection conducted on 7 August 2012:

n Site characteristics: significant liquefaction potential due to widespread liquefaction observed in the surrounding area.



Indicative Building Strength (from Initial Evaluation Procedure and CSW assessment)

The building has been assessed to have a seismic capacity of 36%NBS using the NZSEE Initial Evaluation Procedure (IEP) and is therefore classified as potentially Earthquake Risk and Seismic Grade C.

Recommendations

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be potentially earthquake risk, having an assessed capacity of between 34% and 67%NBS. The risk of collapse of an earthquake risk building is considered to be 5 to 10 times greater than that of an equivalent new building.

No significant damage or hazards were identified to the seismic or gravity load resisting system that would reduce its ability to resist further loads and therefore no restrictions on use or occupancy are recommended.

It is recommended that:

- Purther efforts are made to obtain structural drawings.
- n A verticality and level survey could be carried out to determine the extent of settlement of the building for insurance purposes.
- n Based on the use of the building and the %NBS score we recommend a Quantitative Assessment is carried out to give a more reliable %NBS assessment.
- n Repairs that would bring the building back to an "as new" condition are typically entitled under typical replacement insurance policies. We suggest you consult with your insurance advisor as to how you wish to proceed.



Table of Contents

Qua	alitati	ve Report – SUMMARY	ii
1	Bacl	kground	1
2	Com	npliance	1
	2.1	Canterbury Earthquake Recovery Authority (CERA)	1
	2.2	Building Act	
	2.3	Christchurch City Council Policy	3
	2.4	Building Code	3
3	Eart	hquake Resistance Standards	4
4	Buile	ding Description	5
	4.1	General	5
	4.2	Structural 'Hot-spots'	6
5	Site	Investigations	6
	5.1	Previous Assessments	6
	5.2	Level 4 Damage Inspection	7
6	Dam	nage Assessment	7
	6.1	Damage Summary	7
	6.2	Surrounding Buildings	8
	6.3	Residual Displacements and General Observations	8
	6.4	Implication of Damage	8
7	Gen	eric Issues	8
8	Criti	cal Structural Weaknesses	8
	8.1	Site Characteristics	8
9	Geo	technical Consideration	8
10	Surv	/ey	9
11	Initia	al Capacity Assessment	9
	11.1	%NBS Assessment	9
	11.2	Seismic Parameters	9
	11.3	Expected Structural Ductility Factor	9
	11.4	Discussion of results	10
12	Initia	al Conclusions	10
13	Rec	ommendations	10
	13.1	Occupancy	10
	13.2	Further Investigations, Survey or Geotechnical Work	10
	13.3	Damage Reinstatement	10
14	Desi	ign Features Report	11
15	Limi	tations	11



Appendices

Appendix A - Photographs

Appendix B - CERA DEE Summary Data

Appendix C - Previous Reports and Assessments



1 **Background**

Beca Carter Hollings & Ferner Ltd (Beca) has been engaged by Christchurch City Council (CCC) to undertake a qualitative Detailed Engineering Evaluation (DEE) of the Ascot Community Centre located at 12 Ascot Avenue, Parklands, Christchurch.

This report is a Qualitative Assessment of the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

A qualitative assessment involves inspections of the building, a desktop review of existing structural and geotechnical information, including existing drawings and calculations, if available and an assessment of the level of seismic capacity against current code using the Initial Evaluation Procedure (IEP).

The purpose of the assessment is to determine the likely building performance and damage patterns, to identify any potential Critical Structural Weaknesses or collapse hazards, and to make an initial assessment of the likely building strength in terms of percentage of New Building Standard (%NBS).

At the time of this report, no intrusive site investigation, detailed analysis, or modelling of the building structure has been carried out. No drawings were available and hence this report is based on our visual inspection of the building only.

The format and content of this report follows a template provided by CCC, which is based on the EAG document.

2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

2.1 Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 - Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 – Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee carry out a full structural survey before the building is re-occupied.

We understand that CERA will require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building



Act). It is understood that CERA is adopting the Detailed Engineering Evaluation Procedure document (draft) issued by the Engineering Advisory Group on 19 July 2011, which sets out a methodology for both qualitative and quantitative assessments. We understand this report will be used in response to CERA Section 51.

The qualitative assessment includes a thorough visual inspection of the building coupled with a desktop review of available documentation such as drawings, specifications and IEP's. The quantitative assessment involves analytical calculation of the building's strength and may require non-destructive or destructive material testing, geotechnical testing and intrusive investigation.

It is anticipated that factors determining the extent of evaluation and strengthening level required will include:

- n The importance level and occupancy of the building
- n The placard status that was assigned during the state of emergency following the 22 February 2011 earthquake
- n The age and structural type of the building
- n Consideration of any Critical Structural Weaknesses
- n The extent of any earthquake damage

2.2 **Building Act**

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 - Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to any alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

Section 115 – Change of Use

This section requires that the territorial authority (in this case Christchurch City Council (CCC)) be satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'. Regarding seismic capacity 'as near as reasonably practicable' has previously been interpreted by CCC as achieving a minimum of 67%NBS however where practical achieving 100%NBS is desirable. The New Zealand Society for Earthquake Engineering (NZSEE) recommend a minimum of 67%NBS.

Section 121 – Dangerous Buildings

The definition of dangerous building in the Act was extended by the Canterbury Earthquake (Building Act) Order 2010, and it now defines a building as dangerous if:

- n In the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
- n In the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
- n There is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a 'moderate earthquake' (refer to Section 122 below); or
- n There is a risk that that other property could collapse or otherwise cause injury or death; or
- n A territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.



Section 122 - Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property. A moderate earthquake is defined by the building regulations as one that would generate ground shaking 33% of the shaking used to design an equivalent new building.

Section 124 – Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 - Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

2.3 **Christchurch City Council Policy**

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake of the 4th September 2010.

The 2010 amendment includes the following:

- n A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
- n A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
- n A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
- Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

It is understood that any building with a capacity of less than 33%NBS (including consideration of Critical Structural Weaknesses) will need to be strengthened to a target of 67%NBS of new building standard as recommended by the Policy.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply 'as near as is reasonably practicable' with:

- n The accessibility requirements of the Building Code.
- n The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

2.4 **Building Code**

The building code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.

On 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

a. Hazard Factor increased from 0.22 to 0.3 (36% increase in the basic seismic design load)



b. Serviceability Return Period Factor increased from 0.25 to 0.33 (80% increase in the serviceability design loads when combined with the Hazard Factor increase)

The increase in the above factors has resulted in a reduction in the level of compliance of an existing building relative to a new building despite the capacity of the existing building not changing.

3 Earthquake Resistance Standards

For this assessment, the building's Ultimate Limit State earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The new building standard load requirements have been determined in accordance with the current earthquake loading standard (NZS 1170.5:2004 Structural design actions - Earthquake actions - New Zealand).

No consideration has been given at this stage to checking the level of compliance against the increased Serviceability Limit State requirements.

The likely ultimate capacity of this building has been derived in accordance with the New Zealand Society for Earthquake Engineering (NZSEE) guidelines 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. These guidelines provide an Initial Evaluation Procedure that assesses a building's capacity based on a comparison of loading codes from when the building was designed and currently. It is a quick high-level procedure that can be used when undertaking a Qualitative analysis of a building. The guidelines also provide guidance on calculating a modified Ultimate Limit State capacity of the building which is much more accurate and can be used when undertaking a Quantitative analysis.

The New Zealand Society for Earthquake Engineering has proposed a way for classifying earthquake risk for existing buildings in terms of %NBS and this is shown in Figure 3.1 below.

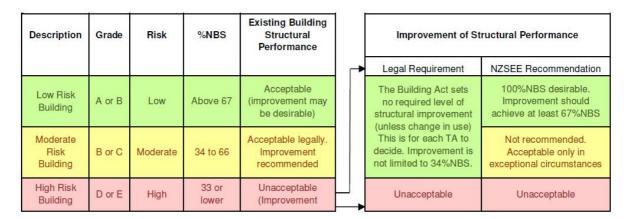


Figure 3.1: NZSEE Risk Classifications Extracted from table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table 3.1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. on average 0.2% in any year). It is noted that the current seismic risk in Christchurch results in a 6% risk of exceedance in the next year.



Table 3.1: %NBS compared to relative risk of failure

Building Grade	Percentage of New Building Standard (%NBS)	Approx. Risk Relative to a New Building
A+	>100	<1
A	80-100	1-2 times
В	67-80	2-5 times
С	33-67	5-10 times
D	20-33	10-25 times
E	<20	>25 times

4 Building Description

4.1 General

Summary information about the building is given in the following table.

Table 4.1: Building Summary Information

Item	Details	Comment
Building name	Ascot Community Centre	
Street Address	12 Ascot Avenue, Parklands, Christchurch	
Age	44 years	Constructed in 1968. Based on a newspaper article about the opening of the building.
Description	The Ascot Community Centre is a multipurpose community space, surrounded by a golf course. The building is generally rectangular in plan and is a single storey structure with the main structural elements being concrete masonry walls.	
Building Footprint / Floor Area	26m x 11m, 290m ² internally	
No. of storeys / basements	1 / No basement	
Occupancy / use	Multipurpose community centre	Importance Level 2 (capacity less than 300)
Construction	The main structural system is concrete masonry walls. Given the age of the building it is likely that the masonry is partially filled and lightly reinforced. The roofing consists of lightweight metal sheeting supported by timber/steel purlins and timber/steel rafters spanning between the external masonry walls.	Based on visual inspection. No drawings available. The roof structure was concealed by the ceiling.



Item	Details	Comment
Gravity load resisting system	The gravity loads from the roof are supported by timber/steel purlins spanning between steel rafters which transmit the load into load bearing concrete masonry walls. Gravity loads from the floor are supported by a concrete slab on grade.	No drawings available.
Seismic load resisting system	The lateral loads in both directions are resisted by the partially filled concrete masonry shear walls. The lateral load from the walls is transmitted into the foundations. It is unknown if there is a concealed roof diaphragm (e.g. timber sarking) or bracing to transmit lateral load from the roof to the walls. Some areas appear to have a fixed plasterboard ceiling which may act as a roof diaphragm.	No drawings available.
Foundation system	Unknown, but assumed to be shallow foundations with a concrete slab on grade.	No drawings available.
Stair system	No stairs	
Other notable features		
External works	Paved and landscaped courtyard.	
Construction information	Visual inspections	No drawings available.
Likely design standard	NZSS 1900 Chapter 8:1965	Inferred from age of building.
Heritage status	Not heritage listed	
Other		

4.2 Structural 'Hot-spots'

- n Connections between the roof diaphragm and the walls.
- n Shear strength of masonry walls.
- n Out of plane capacity of masonry block walls.

5 Site Investigations

5.1 Previous Assessments

The building had a level 2 rapid assessment undertaken following June 2011 earthquake (refer to Appendix C). The June 2011 Rapid Assessment notes that repair works were in progress at the time of the inspection. It is therefore likely that some of the damage caused by the earthquakes is no longer visible.



5.2 **Level 4 Damage Inspection**

Visual inspections as part of the level 4 damage assessment were undertaken on 7 August 2012. Photographs were taken as a record of inspection.

6 **Damage Assessment**

6.1 **Damage Summary**

The table below provides a summary of damage observed during our inspection. Refer to Appendix A for photographs of the observed damage. As noted in Section 5.1 some earthquake damage repair work has been completed.

Table 6.1: Damage Summary

Damage type					Comment
	Unknown	Minor	Moderate	Major	
settlement of foundations	ü				None observed during visual inspection. Level survey may be required to confirm.
tilt of building	ü				None observed during visual inspection. Verticality survey may be required to confirm.
liquefaction	ü				No liquefaction was observed during visual inspection. Aerial photographs taken on 24 February 2011 show there was a high degree of liquefaction observed in the area surrounding the site (refer Appendix A)
settlement of external ground	ü				None observed during visual inspection.
lateral spread / ground cracks	ü				None observed during visual inspection.
frame					No damage observed during visual inspection.
masonry walls					No damage observed during visual inspection. The previous level two assessment noted damage to the masonry walls with repairs underway at the time of the level 2 inspection.
cracking to concrete floors		ü			Minor cracking was observed in the concrete path outside the building.
bracing	ü				Roof bracing, if present, was obscured by the fixed ceiling.
precast flooring seating					Not Applicable
stairs					Not Applicable
cladding /envelope		ü			Minor damage was observed in the ceiling plasterboard lining.
internal fit out					No damage was observed during visual inspection.



Damage type	Unknown	Minor	Moderate	Major	Comment
building services	ü				Building services were not inspected.
other					Not Applicable

6.2 **Surrounding Buildings**

The Ascot Community Centre is adjacent to a golf course and is not in close proximity to any other buildings.

6.3 **Residual Displacements and General Observations**

No evidence of permanent settlement or displacements were observed during our visual inspection, however a global settlement survey may reveal movement that could be described as damage under insurance entitlement.

6.4 Implication of Damage

Other than minor localised cracking in the plasterboard ceiling no superstructure damage was observed during our visual inspection and therefore we believe the structural capacity has not been materially affected.

7 Generic Issues

The following generic issues referred to in Appendix A of the EAG guideline document have been identified as applicable to the Ascot Community Centre:

Partially Filled Concrete Masonry Walls

- n Inadequate shear and/or flexural strength of the concrete masonry walls.
- n Inadequate connection of roof diaphragm to the walls.

8 Critical Structural Weaknesses

Based on the inspection of the building conducted on 7 August 2012 the following Critical Structural Weakness (CSW) was observed.

8.1 Site Characteristics

Based on the aerial reconnaissance on 24 February 2011 evidence of liquefaction was visible on the site. Consequently a significant site characteristic factor of 0.7 representing significant liquefaction was used to assess the %NBS in the IEP assessment of the building.

9 Geotechnical Consideration

No geotechnical information was available for this site. During the inspection, any damage to the surrounding pavement was noted and any affect to the structure was considered.



10 Survey

No level or verticality surveys were carried out as there was no evidence of settlement or displacement observed during the inspection. CCC may wish to undertake a level survey as part of insurance entitlement considerations.

11 Initial Capacity Assessment

11.1 %NBS Assessment

The building has had its seismic capacity assessed using the Initial Evaluation Procedure based on the assumed age, visually determined construction type and assessed structural system. The building's capacity is expressed as a percentage of New Building Standard (%NBS) and is in the order of that shown below in Table 11.1. A factor of 2.5 has been selected for the F factor as the building is a simple single storey structure and no damage other than cracking in the plasterboard ceiling was observed during the inspection (and minor cracking to internal blockwalls which had been repaired prior to inspection). These capacities are subject to confirmation by a quantitative analysis which is more detailed. The post-damage capacity is considered to be the same as the original capacity.

System	Direction	Seismic Performance in %NBS	Notes
Partially filled, reinforced, concrete masonry shear walls.	Longitudinal	36%	NZSEE Initial Evaluation Procedure. IL 2, Z=0.3.
Partially filled, reinforced, concrete masonry shear walls.	Transverse	36%	NZSEE Initial Evaluation Procedure. IL 2, Z=0.3.

Table 11.1: Indicative Building Capacities

11.2 Seismic Parameters

The seismic design parameters based on current design requirements from NZS1170:2004 and the NZBC clause B1 for this building are:

- n Site soil class: D NZS 1170.5:2004, Clause 3.1.3, Soft Soil
- n Site hazard factor, Z = 0.3 NZBC, Clause B1 Structure, Amendment 11 effective from 19 May 2011
- n Return period factor Ru = 1 NZS 1170.5:2004, Table 3.5, Importance level 2 structure with a 50 year design life.
- Near fault factor N(T,D) = 1 NZS 1170.5:2004, Clause 3.1.6, Distance more than 20 km from fault line.

11.3 Expected Structural Ductility Factor

The lateral load resisting system in both directions is partially filled, lightly reinforced concrete masonry shear walls which have been assumed to have a ductility factor of 1.25 in the IEP assessment.



11.4 Discussion of results

Based on the IEP results, the Ascot Community Centre is considered potentially Earthquake Risk and Seismic Grade C as the IEP result is between 33%NBS and 67%NBS. This assessment is qualitative and based on the NZSEE IEP only.

12 **Initial Conclusions**

- n Minor structural earthquake damage observed.
- n The building has been assessed to have a seismic capacity of 36%NBS and is therefore classified as potentially Earthquake Risk.
- n A Critical Structural Weakness has been identified but its impact on the structure is not considered significant.

13 Recommendations

13.1 Occupancy

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be potentially earthquake risk, having an assessed capacity of between 34% and 67%NBS. The risk of collapse of an earthquake risk building is considered to be 5 to 10 times greater than that of an equivalent new building.

No significant damage or hazards were identified to the seismic or gravity load resisting system that would reduce its ability to resist further loads and therefore no restrictions on use or occupancy are recommended.

Further Investigations, Survey or Geotechnical Work

It is recommended that:

- n A verticality and level survey could be carried out to determine the extent of settlement of the building for insurance purposes.
- n Given the community use of the building a quantitative assessment should be undertaken to give a more reliable assessment of %NBS.
- Purther efforts are made to obtain structural drawings.

13.3 Damage Reinstatement

Repairs that would bring the building back to an "as new" condition are typically entitled under typical replacement insurance policies. We suggest you consult with your insurance advisor as to how you wish to proceed.



14 **Design Features Report**

Repairs will be required to reinstate the existing structural system. No new load paths are expected. A repair methodology has not been prepared at this stage.

15 Limitations

The following limitations apply to this engagement:

- n Beca and its employees and agents are not able to give any warranty or guarantee that all defects, damage, conditions or qualities have been identified.
- n Inspections are primarily limited to visible structural components. Appropriate locations for invasive inspection, if required, will be based on damage patterns observed in visible elements, and review of the construction drawings and structural system. As such, there will be concealed structural elements that will not be directly inspected.
- n The inspections are limited to building structural components only.
- Inspection of building services, pipework, pavement, and fire safety systems is excluded from the scope of this report.
- n Inspection of the glazing system, linings, carpets, claddings, finishes, suspended ceilings, partitions, tenant fit-out, or the general water tightness envelope is excluded from the scope of this report.
- n The preliminary assessment of the lateral load capacity of the building is limited by the completeness and accuracy of the drawings provided. Assumptions have been made in respect of the geotechnical conditions at the site and any aspects or material properties not clear on the drawings. Where these assumptions are considered material to the outcome further investigations may be recommended. It is noted the assessment has not been exhaustive, our analysis and calculations have focused on representative areas only to determine the level of provision made. At this stage we have not undertaken any checks of the gravity system, wind load capacity, or foundations.
- n The information in this report provides a snapshot of building damage at the time the detailed inspection was carried out. Additional inspections required as a result of significant aftershocks are outside the scope of this work.

This report is of defined scope and is for reliance by CCC only, and only for this commission. Beca should be consulted where any question regarding the interpretation or completeness of our inspection or reporting arises.



Appendix A

Photographs



Figure 1: Site layout



Photo 1: External view of the building



Photo 2: Liquefaction of areas surrounding site (aerial photo taken 24 February 2011)



Photo 3: Internal view of the building

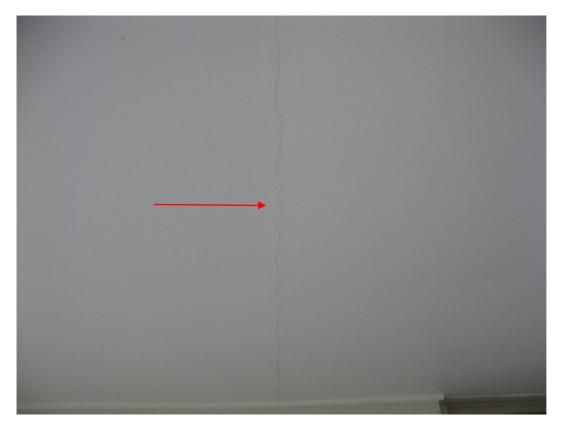


Photo 4: Damage to plasterboard ceiling

Damage: Minor cracking (<1mm) to plasterboard ceiling panels.



Photo 5: External concrete pavement

Damage: Minor cracking to concrete slab.

Appendix B

CERA DEE Summary Data

Detailed Engineering Evaluation Summary Data				V1.11
Location				
Building Name:	: Ascot Community Centre Unit	No:	Street Reviewer: CPEng No:	David Whittaker 123089
Building Address: Legal Description:		12	? Ascot Avenue, Parklands Company: Company project number:	Beca 5323355
			Company phone number:	
GPS south:		IVIII	Date of submission:	14/06/2013
GPS east:			Inspection Date: Revision:	7/08/2012 A
Building Unique Identifier (CCC):	BU 1306-003		Is there a full report with this summary?	yes
Site				
Site slope:			Max retaining height (m):	0
Soil type: Site Class (to NZS1170.5):	D		Soil Profile (if available):	Unknown
Proximity to waterway (m, if <100m): Proximity to clifftop (m, if < 100m):			If Ground improvement on site, describe:	N/A
Proximity to cliff base (m,if <100m):			Approx site elevation (m):	
Building				
No. of storeys above ground: Ground floor split?	: 1 no		single storey = 1 Ground floor elevation (Absolute) (m): Ground floor elevation above ground (m):	0.00
Storeys below ground	d 0 other (describe)		if Foundation type is other, describe:	Shallow Foundations
Building height (m):	5.00		height from ground to level of uppermost seismic mass (for IEP only) (m):	5
Floor footprint area (approx): Age of Building (years):			Date of design:	1965-1976
Strengthening present?	no		If so, when (year)?	
Use (ground floor):	other (specify)		And what load level (%g)? Brief strengthening description:	
Use (upper floors):	: General purpose community centre			
Importance level (to NZS1170.5):				
Gravity Structure				
Gravity System:	load bearing walls			
Floors	steel framed other (note)			Shallow foundations
	timber load bearing walls		type typical dimensions (mm x mm)	
Walls:	partially filled concrete masonry		thickness (mm)	
Lateral load resisting structure				
Lateral system along. Ductility assumed, µ:	: partially filled CMU 1.25		Note: Define along and across in detailed report! note total length of wall at ground (m):	26
Period along	0.40	####	enter height above at H31 estimate or calculation?	estimated
Total deflection (ULS) (mm): maximum interstorey deflection (ULS) (mm):			estimate or calculation? estimate or calculation?	
				44
Lateral system across: Ductility assumed, μ:	: partially filled CMU		note total length of wall at ground (m):	11
Period across: Total deflection (ULS) (mm):		####	enter height above at H31 estimate or calculation? estimate or calculation?	estimated
maximum interstorey deflection (ULS) (mm):	4		estimate or calculation?	
Separations:				
north (mm): east (mm):			leave blank if not relevant	
south (mm):	:			
west (mm):				
Non-structural elements Stairs:				none
Wall cladding:	: exposed structure		describe	Concrete masonry walls
Roof Cladding: Glazing:	: timber frames		describe	Lightweight metal sheeting
Ceilings: Services(list):	: plaster, fixed : Electrical, Plumbing			
Available documentation				
Architectural Structural			original designer name/date original designer name/date	
Mechanical	I none		original designer name/date	
Electrical Geotech report	none		original designer name/date original designer name/date	
Damage				
Site: Site performance: (refer DEE Table 4-2)			Describe damage:	
Settlement: Differential settlement:	none observed none observed		notes (if applicable): notes (if applicable):	
				Aerial photos showed liquefaction
Lateral Spread:	: 2-5 m³/100m² : none apparent		notes (if applicable):	occurred in surrounding area
Differential lateral spread	: none apparent : none apparent		notes (if applicable): notes (if applicable):	
Damage to area:	none apparent		notes (if applicable):	
Building:				
Current Placard Status	green			
				Damage not considered to have reduced
Along Damage ratio: Describe (summary):			Describe how damage ratio arrived at:	capacity
		Da	$mage _Ratio = \frac{(\% NBS (before) - \% NBS (after))}{(\% NBS (before))}$	
Across Damage ratio: Describe (summary):		Du	mage _ Kano = % NBS (before)	
Diaphragms Damage?:	: no		Describe:	
CSWs: Damage?:			Describe:	
IDamadiaa.	no		Describe:	
Pounding: Damage?:			Describe:	Minor cracking to plasterboard ceilings
Non-structural: Damage?:	yes			
Non-structural: Damage?:	: yes			
Non-structural: Damage?:				Repair cracking to plasterboard
Non-structural: Damage? Recommendations Level of repair/strengthening required Building Consent required	: minor structural		Describe:	Repair cracking to plasterboard
Non-structural: Damage? Recommendations Level of repair/strengthening required Building Consent required Interim occupancy recommendations	minor structural no [full occupancy		Describe: Describe:	Repair cracking to plasterboard
Non-structural: Damage?: Recommendations Level of repair/strengthening required Building Consent required Interim occupancy recommendations Along Assessed %NBS before e'quakes	iminor structural no ltill occupancy	36%	Describe: Describe: 9 %NBS from IEP below If IEP not used, please detail assessment	Repair cracking to plasterboard
Non-structural: Damage?: Recommendations Level of repair/strengthening required Building Consent required Interim occupancy recommendations Along Assessed %NBS before e'quakes Assessed %NBS after e'quakes	minor structural no full occupancy 36%		Describe: Describe: NNBS from IEP below If IEP not used, please detail assessment methodology:	Repair cracking to plasterboard
Non-structural: Damage?: Recommendations Level of repair/strengthening required Building Consent required Interim occupancy recommendations Along Assessed %NBS before e'quakes	minor structural no [tull occupancy] 36% 36%		Describe: Describe: 9 %NBS from IEP below If IEP not used, please detail assessment	Repair cracking to plasterboard

IEP	Use of this method is not mandatory - more detailed analysis	may give a different answer, which woul	ld take precedence. Do not fill i	n fields if not usi	ng IEP.
	Period of design of building (from above): 1965-1976		h₁ from above:	5m	
Soiomio -	one, if designed between 1965 and 1992: B		not required for this age of building		
Seisifiic 2	one, il designed between 1903 and 1992.		not required for this age of building		
			along		across
		Period (from above):	0.4 5.0%		0.4 5.0%
		(%NBS)nom from Fig 3.3:			
	Note:1 for specifically design public buildings, to the code of the day: pre-		35-1976, Zone B = 1.2; all else 1.0 gned between 1976-1984, use 1.2		1.00
		Note 3: for buildings designed prior to 1935 u	use 0.8, except in Wellington (1.0)		1.0
			along		across
		Final (%NBS)nom:	5%		5%
	2.2 Near Fault Scaling Factor	Near Fault scaling	g factor, from NZS1170.5, cl 3.1.6: along		1.00 across
	Near Faul	t scaling factor (1/N(T,D), Factor A:	1		1
	2.3 Hazard Scaling Factor	Hazard factor Z	for site from AS1170.5, Table 3.3:		0.30
			Z ₁₉₉₂ , from NZS4203:1992 Hazard scaling factor, Factor B:	2.0	0.8 333333333
			riazaiu scaiiig iactor, ractor B.	3.0	3333333
	2.4 Return Period Scaling Factor	Build	ding Importance level (from above):		2
	2.4 Notain Fortor occuring Factor		ng factor from Table 3.1, Factor C:		1.00
			along		across
		ductility (less than max in Table 3.2)	1.25		1.25
	Ductility scaling factor: =1 from 1976 onwards		1.14		1.14
		Ductiity Scaling Factor, Factor D:	1.14		1.14
	2.6 Structural Performance Scaling Factor:	Sp:	0.925		0.925
	Structural Pe	erformance Scaling Factor Factor E:	1.081081081	1.0	081081081
	2.7 Baseline %NBS, (NBS%)b = (%NBS)nom x A x B x C x D x E	%NBS _b :	21%		21%
	Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)				
	3.1. Plan Irregularity, factor A:				
	3.2. Vertical irregularity, Factor B:				
		Table for selection of D1	Severe	Significant	Insignificant/none
	3.3. Short columns, Factor C:	Separ		05 <sep<.01h< th=""><th>Sep>.01H</th></sep<.01h<>	Sep>.01H
	3.4. Pounding potential Pounding effect D1, from Table to right 1.0	Alignment of floors within 20%	of H 0.7	0.8	1
	Height Difference effect D2, from Table to right 1.0	Alignment of floors not within 20%	of H 0.4	0.7	0.8
	Therefore, Factor D: 1	Table for Selection of D2		Significant	Insignificant/none
	3.5. Site Characteristics significant 0.7	Separ		05 <sep<.01h< th=""><th>Sep>.01H</th></sep<.01h<>	Sep>.01H
		Height difference > 4 sto Height difference 2 to 4 sto		0.7	1
		Height difference < 2 sto		1	1
			Along		Across
		erwise max valule =1.5, no minimum	2.5		2.5
	Ra	tionale for choice of F factor, if not 1 Simple s	single storey structure, only minor damage	sustained	
	Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)				
	List any: Refer a	llso section 6.3.1 of DEE for discussion of F	factor modification for other critical	structural weakne	sses
	3.7. Overall Performance Achievement ratio (PAR)		1.75		1.75
	4.3 PAR x (%NBS)b:	PAR x Baselline %NBS:	36%		36%
	· ´				
	4.4 Percentage New Building Standard (%NBS), (before)				36%
Official Use only					
	Accepted By Date:				
	Date.				

Appendix C

Previous Reports and Assessments

·					
Inspector Initials Territorial Authority	Sichurch Equation Christchurch City	Date of Inspection	-///-	Exterior Only Exterior and Interior	
Building Name Short Name Address	Ascot Con- 50 1306-00 193 Travis	Type	of Construction Timber frame Steel frame	Concrete shear wall	
GPS Co-ordinates Contact Name Contact Phone	S° E°		Tilt-up concrete Concrete frame RC frame with masonry infill	Unreinforced masonry Reinforced masonry Confined masonry Other:	
Storeys at and above ground level Total gross floor area (m²) No of residential Units Photo Taken	Below groulevel Year built Yes No	1968 D	ny Occupancy Dwelling Other residential Public assembly School Religious	Commercial/Offices Industrial Government Heritage Listed Other	1
Investigate the building for Overall Hazards / Damag Collapse, partial collapse, off Building or storey leaning Wall or other structural dama Overhead falling hazard Ground movement, settlement Neighbouring building hazard Other	ge Minor/Non foundation age at, slips		Severe		mason
UNSAFE posting, main entrance, Posting entrance, Posting Record any restriction Record any restriction Record and Earticades are Level 2 or def	Localised Severe and over all other placards at eve INSPECTED GREEN ction on use or entry: ecommended: low only if further actions are a needed (state location): alled engineering evaluation uctural	rall Moderate conditions y significant entrance. RES	ns may require a RESTRIC	the whole building are grounds TED USE. Place INSPECTED pla UNSAFE RED	
Estimated Overall Buildi None	ng Damage (Exclude Co 31-60 % 61-99 % 100 %,		Data ID	Sign here on completion 18/6/2 2019	

Gnisignuren er RAPID Assessmen Eonnel EVEL 2 Final Posting Date Inspector Initials (e.g. UNSAFE) Time Christchurch City Territorial Authority **Building Name** Type of Construction Short Name Concrete shear wall Timber frame Address Unreinforced masonry Steel frame Reinforced masonry Till-up concrete **GPS Co-ordinates** Confined masonry Concrete frame Contact Name Other: RC frame with masonry Infill Contact Phone Primary Occupancy Below Commercial/Offices Storeys at and above ground Dwelling ground level level Industrial Year Total gross floor area Other residential built (m²)Government Public assembly No of residential Units Heritage Listed School Other Religious No Photo Taken Yes Investigate the building for the conditions listed on page 1 and 2, and check the appropriate column. A sketch may be added on page 3 Severe Moderate Minor/None Overall Hazards / Damage Collapse, partial collapse, off foundation . Building or storey leaning П Wall or other structural damage Overhead falling hazard П Ground movement, settlement, slips П Neighbouring building hazard П Electrical, gas, sewerage, water, hazmats Existing Record any existing placard on this building: Placard Type (e.g. UNSAFE) Choose a new posting based on the new evaluation and team judgement. Severe conditions affecting the whole building are grounds for an UNSAFE posting. Localised Severe and overall Moderate conditions may require a RESTRICTED USE. Place INSPECTED placard at main entrance. Post all other placards at every significant entrance. Transfer the chosen posting to the top of this page. UNSAFE RESTRICTED USE INSPECTED R3 R2 R1 RED Y2 YELLOW GREEN G1 G2 Record any restriction on use or entry: Further Action Recommended: Tick the boxes below only if further actions are recommended ☐ Barricades are needed (state location): ☐ Detailed engineering evaluation recommended Other: ☐ Geotechnical ☐ Structural ☐ Other recommendations: Sign here on completion Estimated Overall Building Damage (Exclude Contents) None · 31-60 % 0-1 % Date & Time 61-99 % 2-10 % 100 % 11-30 % П Inspection ID: _____ (Office Use Only) PRUPI:

Structural Hazards/ Damage Foundations Roofs, floors (vertical load) Columns, pilasters, corbels Diaphragms, horizontal bracing Pre-cast connections Beam Non-structural Hazards / Damage Parapets, ornamentation Cladding, glazing Ceilings, light fixtures Interior walls, partitions Elevators Stairs/ Exits Utilities (eg. gas, electricity, water) Other Geotechnical Hazards / Damage Slope failure, debris Ground movement, fissures Soll bulging, liquefaction		Minor/None Dadadadadadadadadadadadadadadadadadada	Moderate O O O O O O O O O O O O O O O O O O O	Severe	minor ropair works in process to block willy t ceiling. I gun fection on street rearby-
General Comment			•		
Usability Category					
Damage Intensity	Posting		ility Category		Remarks
Light damage	Inspected	G1. Occuplabl Investigat	e, no immediate i ion-required	iurther	a in process of
Low risk	(Green)	G2. Occupiab	e, repairs require	d)	7 in process of
Medlum damage	Restricted Use	Y4. Short-term-entry			
Medium risk	(Yellow)	Y2. No entry t demolish	o parts until repal ed	red or	
	Unsafe (Red)	R1. Significan strengthe	t damage: repairs ning possible	1	
Heavy damage High risk		R2. Severe da	amage: demolition	ı likely	
		R3. At risk fro from grot	m adjacent preml und fallure	ses or	·

Sketch (optional)
Provide a sketch of the entire
building or damage points. Indicate
damage points.

							:		
<u> </u>					 				
								ŀ	
				 		<u> </u>	<u> </u>		
		-	 						
								<u>. </u>	
									ł.
	-					 <u> </u>			
				ļ		 			
						}			
				 	 <u> </u>	 <u></u>	1	<u></u>	L

Recommendations	for Repair and Reconstruction or Demolition (Optional)